Civil UAV Type Certification: DoD Mishap Analysis 2000-2009 and FAA Certification Roadmap

By

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UAV FAA Airworthiness, Mishap Trends, Incident Trends, Certification, 14CFR Part 23, Part 23, 14CFR Part 25

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Abstract

The Federal Aviation Administration (FAA) has issued memorandums which support the use of flight activities which can demonstrate that proposed operation can be conducted at an acceptable level of safety. This paper examines the existing data available from the Air Force on Unmanned Air System (UAS) reliability, and attempts to apply that information to UAS FAA certification. This will allow UAS to operate more freely in the National Airspace System (NAS).

The current state of UAS operations is assessed from the Safety Investigation Board One-Line Summaries and Judge Advocate General Accident Investigation Board executive summaries. This data is categorized and aggregated to show sources of failure and the impact of those failures on the system. Detail failure trends are derived from the data that show gaps in airworthiness. This data is then tested against the applicable subset of Part 25 rules for sufficiency as a Means of Compliance (MOC). The gaps in sufficiency are discussed, and alternative methods for knowledge acquisition are examined for their sufficiency as MOC. The uniqueness of UAS safety, new risks and reduced risk, is discussed finally, and a plan is proposed to reduce certification burden in a post-production environment for this new Type Class of Vehicle. The result is a hypothetical set of UAS rules and means of compliance that supports UAS incorporation in the NAS by the 2015 deadline specified in recent federal law.

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List of Abbreviations

14CFR	Title 14 of the Code of Federal Regulations – Aeronautics and Space
49CFR	Title 49 of the Code of Federal Regulations - Transportation
AIB	Accident Investigation Board
AFSC	Air Force Safety Center
CAA	Civil Aeronautic Authority
COA	Certificate of Wavier or Authorization
FAA	Federal Aviation Administration
DoD	Department of Defense
HALE	High Altitude Long Endurance
MALE	Medium Altitude Long Endurance
MOC	Means of Compliance
NAS	National Airspace System
Part 23	14CFR Part 23 – Airworthiness Standards: Normal, Utility, Acrobatic, and Commuter Category Airplanes
Part 25	14CFR Part 25 – Airworthiness Standards: Transport Category Airplane

Part 26	14CFR Part 26 - Airworthiness and Safety Improvements for Transport Category
	Airplanes

- Part 33 14CFR Part 33 Airworthiness Standards: Aircraft Engines
- Part 35 Airworthiness Standards: Propellers
- SIB Safety Investigation Board
- RPV Remotely Piloted Vehicles
- Title 10 U.S. Code Title 10 Armed Forces
- TC Type Class
- UAV Unmanned Air Vehicle
- UAS Unmanned Air System

Causation Categories:

- LL Lost Link
- RP Reduced Perception
- HL Hard Landing
- RE Reliability
- PE Pilot Error
- ME Maintenance Error

ENV Environmental

=== Unclassified

Reliability Categories:

PWP Power Plant

- AP Auto Pilot
- EE Electrical
- HD Hydraulic
- STR Structural

1. Background

The Federal Aviation Administration (FAA) has an over arching goal to ensure the airworthiness of aircraft flying in the National Airspace (NAS). Typically, this airworthiness is demonstrated during the engineering design and initial testing of a new system. Policy and regulation dictate that for a new system to have access to the NAS, that system must demonstrate an acceptable level of safety. This safety assessment must conform to the existing set of regulations presented in Title 14 of the Code of Federal Regulations – Aeronautics and Space (14CFR). These regulations have been developed over time to ensure the air system designers address airworthiness issues that have affected aircraft safety in the past and to ensure that all vehicles in the market are starting from the same minimal level of safety required to sustain the operational confidence necessary for a large air commerce system to exist.

However, there are situations where aircraft move though design, manufacturing, and flight test phases with limited FAA involvement (e.g., agricultural, experimental, and military aircraft). In these situations, such aircraft are flown in a highly restrictive manner or certified for flight by a body outside the FAA (i.e., the Department of Defense (DoD)). Unmanned air systems (UAS) are such systems.

Such evolution of a system, outside FAA certification, is not unprecedented. UAS are now moving down a path similar to certification as agricultural aircraft after the dawn of aviation. These aircraft were developed prior to the codification of civil air regulations and presented a challenge to certification under the new rules. Their barn storming developmental roots was compensated for by the restriction of the space they operated in. The risk created by these barn built amateur aircraft was deemed completely segregated from non-consenting citizens. The pilot consented to operation of this experimental airframe, and the landowner

consented to its operation on his property. Today, agricultural planes are certified to 14CFR Part 23 – Airworthiness Standards: Normal, Utility, Acrobatic, and Commuter Category Airplanes (Part 23) minus a list of allowed exemptions that the Administrator found inappropriate for that aircraft Type.

UAS have moved beyond niche systems, and their success has suggested numerous applications beyond the DoD. Future unrestricted use of UAS in the NAS will therefore require some form of "catch up" certification to account for those activities that were not conducted jointly with the FAA during design, manufacture, and initial certification of the small fleet of large UAS whose operational reliability would impact the safety of the NAS. To accomplish post-production certification, the FAA has issued memorandums which support the use of flight activities which can demonstrate that proposed operation can be conducted at an acceptable level of safety. This implies that some form of risk assessment can be applied to proposed operations by making use of data from fleet operations that would offset the amount of supplement testing and observation required to prove airworthiness.

This thesis examines the available data from two sources of operational activity between FY2000-FY2009. The thesis looks to the data for use in certification of the Large UAS in question, and proceeds with an assessment of the current safe level of these systems based on that data. This paper outlines a process by which UAS certification for operations in the NAS could be achieved. Based on the existing training of pilot and crew, the technology depended on for navigation, and the graceful mission of the UAS in question, the transport rules of Part 25 are the most applicable to current Medium and High Altitude Long Endurance (MALE and HALE) UAS. These regulations could be applied to a UAS minus a list of exemptions that account for the reduced safety risk posed by UAS. The existing fleet data is reviewed for its sufficiency in

fulfilling the remaining applicable Part 25 rules, and supplemental means of compliance are discussed that would fulfill the remaining certification burden that exists for these aircraft with the anticipation of their operation in the NAS under the 2015 mandate.

1.1. UAVs Examined in This Study

1.1.1. Predator

The RQ-1 first entered service in April of 1996. It is the earliest and smallest system of interest to this study. It has a wing span of 55 ft, 1130 lb dry weight, and a max payload of 450 lbs. The original mission of the RQ-1 is intelligence, surveillance, and reconnaissance. The "R" is a Department of Defense designation for reconnaissance aircraft. The "Q" designates an unmanned system, and the "1" designate that is the first remotely piloted vehicle fielded by the DoD. In 2002, the fleet began conversion to "MQ-1". This came with the addition of 2 Hard Points. Most popularly used for the attachment of two 110lb Hellfire missiles. The "M" is the DoD designation for multi-role. A general summary of MQ-1B specs can be found below in Table 1.1.1.1. To get a better grasp of scale, the predator RQ-1 is shown with personnel in Figure 1.1.1.1. (1)

Contractor: General Atomics Aeronautical Systems Inc. **Power Plant:** Rotax 914F four cylinder engine Power: 115 horsepower Wingspan: 55 feet (16.8 meters) Length: 27 feet (8.22 meters) **Height:** 6.9 feet (2.1 meters) Weight: 1,130 pounds (512 kilograms) empty Maximum takeoff weight: 2,250 pounds (1,020 kilograms) Fuel Capacity: 665 pounds (100 gallons) **Payload:** 450 pounds (204 kilograms) Speed: Cruise speed around 84 mph (70 knots), up to 135 mph **Range:** Up to 770 miles (675 nautical miles) Ceiling: Up to 25,000 feet (7,620 meters) Armament: Two laser-guided AGM-114 Hellfire missiles Crew (remote): Two (pilot and sensor operator) Table 1.1.1.1 – MQ-1B System Specifications. (1)



Figure 1.1.1.1 – RQ-1 Predator Drone being taxied by personnel

1.1.2. Reaper

The MQ-9 Reaper first entered service February 2001. Sometimes it is called the Predator B. It is a scaled up version of the MQ-1 Predator. The wing span is increased to 66 ft. The power plant is upgraded to a Honeywell TPE331-10GD turbo prop producing 900 hp. The dry weight rose considerably considering the 20% increase is span. This is mostly due to an increase in fuselage size and wing reinforcement. The dry weight is 4,900lbs enabling a payload increase to 3,750 lbs. This aircraft is designed from day one to carry munitions. The primary role of this system is hunter/killer. Unlike the MQ-1, which was retrofit 6 years into service, the MQ-9 has 6 hard mounts to carry mostly Hellfires and JDAMs. The general specifications of the MQ-9 are found in Table 1.1.2.1. A picture of the Reaper next to personnel is shown in Figure 1.1.2.1 for perspective. (2)

Primary Function: Remotely piloted hunter/killer weapon system Contractor: General Atomics Aeronautical Systems, Inc. Power Plant: Honeywell TPE331-10GD turboprop engine Max Power: 900 shaft horsepower Wingspan: 66 feet (20.1 meters) **Length:** 36 feet (11 meters) Height: 12.5 feet (3.8 meters) Weight: 4,900 pounds (2,223 kilograms) empty Maximum takeoff weight: 10,500 pounds (4,760 kilograms) Fuel Capacity: 4,000 pounds (602 gallons) **Payload:** 3,750 pounds (1,701 kilograms) **Speed:** Cruise speed around 230 miles per hour (200 knots) **Range:** 1,150 miles (1,000 nautical miles) **Ceiling:** Up to 50,000 feet (15,240 meters) Armament: Combination of AGM-114 Hellfire missiles, GBU-12 Paveway II and GBU-38 Joint Direct Attack Munitions Crew (remote): Two (pilot and sensor operator) Table 1.1.2.1 – MQ-9 System Specifications (2)



Figure 1.1.2.1 – MQ-9 being taxied by personnel.

1.1.3. Global Hawk

The RQ-4 is the largest UAS in service as of the end of this study. It has a wingspan of 112ft and Rolls-Royce-North American F137-RR-100 turbofan engines. The payload is less than the MQ-9 at only 3,000lbs. This gives the aircraft unparalleled high altitude, long endurance capability. Its primary function is intelligence, surveillance, and reconnaissance. None of the aircraft in the study were weaponized. It first flew in 1995 as an Advanced Concept Prototype and is intended as a superior replacement to the U-2 spy plane. The general specifications for the RQ-4 are found in Table 1.1.3.1. A picture of the Global Hawk next to personnel is shown as Figure 1.1.3.1 for perspective. (3)

Primary function: High-altitude, long-endurance ISR Contractor: Northrop Grumman (Prime), Raytheon, L3 Comm Power Plant: Rolls Royce-North American F137-RR-100 turbofan engine Thrust: 7,600 pounds Wingspan: 130.9 feet (39.8 meters) Length: 47.6 feet (14.5 meters) Height: 15.3 feet (4.7 meters) Weight: 14,950 pounds (6,781 kilograms) Maximum takeoff weight: 32,250 pounds (14628 kilograms) Fuel Capacity: 17,300 pounds (7847 kilograms) **Payload:** 3,000 pounds (1,360 kilograms) **Speed:** 310 knots (357 mph) **Range:** 8,700 nautical miles **Ceiling:** 60,000 feet (18,288 meters) Armament: None **Crew (remote):** Three (LRE pilot, MCE pilot, and sensor operator) Table 1.1.3.1 – RQ-4 Global Hawk System Specifications (3)



Figure 1.1.3.1 – RQ-4 Global Hawk being taxied by personnel.

1.2. FAA

The FAA mission is to provide the safest, most efficient aerospace system in the world. The FAA certifies all aircraft, airlines, and airmen that operate in the Nation Airspace System (NAS). For more than five decades, the Federal Aviation Administration has compiled a proven track record of introducing new technology and aircraft safely into the NAS. Most recently, the agency is working to ensure the safe integration of UAS in the NAS. The FAA's sole mission and authority, as it focuses on the integration of unmanned aircraft systems, is safety. Title 14 – Aeronautics and Space already exists to govern the operations of the FAA, how it makes rules, and the minimum design and operation standards that govern all existing aircraft that operate in the NAS. The FAA already is already moving forward with procedures and standards to allow operation of very small and small publicly operated UAS in the NAS. These aircraft all weigh less than 25 lbs and operate at altitudes less than 400 feet, 5 miles away from airports, and within line of sight (AC91-57). These rules do not apply to the aircraft reviewed in this study. The large UAS, operated primarily by the military, are too large to be governed by recent rules and are not allowed to operate freely in the NAS. The FAA currently requires application for one-time Certificate of Wavier or Authorization (COA) for each Large UA operating is the NAS. These COA dictate a time restricted operation window and a chaser aircraft to escort the aircraft through the airspace maintaining visual line of site. The airspace is shut down in sequential blocks to keep the UA segregated from manned air traffic. This procedure prohibits routine access to the NAS by the non-certified UAS.

The National Defense Authorization Act and the 2012 FAA Reauthorization Act mandates that UAS will be integrated into the NAS by 2015 (10). For this to happen, two things must happen. Rules must be drafted to regulate the safety of unmanned system in design, construction, and operation; a new part to address this new Type Class of aircraft currently not allowed or governed, UAS. Second, to show that these new aircraft meet the to-be drafted standard, there must be Means of Compliance (MOC) to these rules. These means come in the form of data that show a certain level of proof, which supports the applicant's claims of airworthiness. The level of proof necessary should also be reviewed in the context of UAS reduced risk to minimize certification burden. In the end, the FAA has sole authority to approve the design, construction, and operation of air vehicles operating in the NAS.

1.3. NAS

The National Airspace exists over the United State, its Territories, and much of the surrounding ocean. This volume is under the sole authority of the FAA. This airspace is divided in to different Classes of airspace labeled A-G to facilitate operation of different levels of aircraft technology and handle the densest traffic spaces efficiently and safely. The FAA also designates

restricted airspace that is handed over to other authoritative bodies (e.g. DoD, DoE) for security, experimentation, and training purposes. By the powers delegated in Title 49, the FAA has the authority to determine the risk of all non-authorized vehicles in the airspace and shutdown airspace around these vehicles in proportion to the perceived threat to protect the flying public from harm. This includes vehicles operated by the DoD. The DoD has authority under Title 10 of the United States Code to operate with only regard to presidential authority during "defense of territory". These conflicting authorities allow the current standoff in UAS operation in the NAS.

1.4. AFSC

Because the DoD operates outside the FAA, it has its own internal safety agency, the Air Force Safety Center (AFSC). The AFSC in a new organization, activated in 1996 (8) which consolidated all safety functions of USAF at Kirtland AFB, in Albuquerque, NM. The organization's mission is to prevent mishaps, and preserve combat capability. The center oversees mishap investigations, evaluates corrective actions, and ensures implementation of these actions. The AFSC also maintain the mishap database for USAF. This database contains all the Safety Investigation Board (SIB) reports. These boards are convened under the authority of AFI 91-204(4). These are privileged (classified) reports that extensively describe the details of each mishap. These mishaps are categorized in classes A through E. Class A is the most severe meaning the mishap resulted in fatality, total disability, more than a million in private property damages, or total loss of vehicle. Because of the nature of this study and in defense to the concept of privilege, the Auburn research team was never granted access to the full SIB reports. Instead, the AFSC sent "One Line Descriptions" of the Mishap cause and resulting UA damage. This is a severe reduction in information. The original SIB reports are 10-20 pages in length. An example of an AFSC data Element is shown in Table 1.4.1.

RPA ID Number	43	
Fiscal Year	2009	
Mishap Class	С	
Accident Category	Aviation	
Accident Sub-category	Unmanned Aerial Vehicle	
One-liner Description	MQ-1; OIL LOSS; ENGINE	
	DESTROYED	
Additional Damage Description	Aircraft engine was destroyed	
This RPAs Age	11	
Total Number of RPAs This FY	171	
This FY Fleet Avg Age (YRS) of This	5.8	
Model RPAs		
MDS Category	RPA	
Visibility Conditions	Visual Meteorological Conditions	
	(VMC)	
Operational Contingency	Yes	
WX Note:	Dust/Ash	
Additional Note:		

Table 1.4.1 – Sample Data Elements Available from the Air Force Safety Center

1.5. AIB

Accident Investigation Boards are convened under the authority of AFI 51-503(8). These committees are assembled to investigate all Class A accidents. These investigations are completely separate from the SIB investigation. The purposes of these AIB investigations are to provide a publicly-releasable report of the facts and the circumstances surrounding the accident, to include a statement of opinion on the cause or causes of the accident, and to gather and preserve evidence for claims, litigation, disciplinary, and adverse administrative actions. In contrast, the primary purpose of a SIB investigation is to find the cause of an accident in order to take preventative action. The AIB report summaries being publically available provided a wealth of information beyond that originally released by the AFSC. The ASFC data we received was approximately 2-4 sentences of narrative material per mishap while the AIB summaries are

approximately 300-500 words. Without the incomparable detail of these summaries, the detailed case studies and trend analysis would not have been possible. It is important to note that these AIB summaries had to be found independent of the AFSC. It is also important to note that the count of Class A UAS incidence between FY2000-FY2009 are different. To date the number of AIB reports are too incomplete to provide meaningful assessment of MQ-9 reliability. Only 2 reports have been published for MQ-9 while 9 Class A incidences are listed in the AFSC data set. Also, the AFSC data does not contain tail numbers or precise mishap dating. This intentional ambiguity makes correlation of AIB mishaps to AFSC mishaps unreliable. Acquisition of the remaining AIB reports would be a meaningful follow on work.

EXECUTIVE SUMMARY AIRCRAFT ACCIDENT INVESTIGATION MQ-IB PREDATOR S/N 03-3112 DEPLOYED LOCATION 17 January 2007

On 17 January 2007 at 2035Z, an MQ-1B PREDATOR, S/N 03-3112, 15th Reconnaissance Squadron, Creech AFB, Nevada, crashed during a reconnaissance mission while operating from a deployed location in the Central Command Area of Responsibility. Upon ground impact, the unmanned aircraft was severely damaged with losses valued at \$4,160,391.00 No one was injured in the accident. Other than the Mishap Aircraft (MA), there was no damage to government or private property. There was very limited media interest. Approximately 14 hours into a 20 hour sortie, the aircraft sustained a momentary (two (2) seconds) drop in engine rotations per minute (RPM) followed 15 minutes later by catastrophic engine failure. Data logger analysis of changes in RPM, oil pressure, turbo oil temperature, and propeller pitch subsequent to the original two second RPM drop indicate the engine was failing over a period of approximately 15 minutes. However, monitored engine parameters remained within normal ranges until approximately the last minute before the engine seized. Therefore, the MA did not generate any form of caution or warning to the pilot of the impending failure until approximately 60 seconds prior to the engine completely failing.

There is clear and convincing evidence that the first point of failure was a crack in the crankshaft which propagated over time to the area of the #4 connecting rod bearing. The # 4 connecting rod ultimately failed and wedged itself in the opposing #3 cylinder causing the crankshaft to immediately stop approximately 15 minutes after the initial two second drop in engine RPM.

The pilot took appropriate actions to establish a glide to an unpopulated area with the intent to land the MA via KU band (satellite) control. By telephone, the Combined Air Operations Center (CAOC) directed the Mission Commander (MCC) to crash the MA rather than attempt a landing if there were no friendly personnel to secure the aircraft. The CAOC decision was based on the classified equipment the MA was carrying and the two Hellfire missiles. The CAOC determined that there were no friendly forces to secure the MA on the ground nearby so the Mishap Pilot 2 (MP2) intentionally crashed the MA into an unpopulated area. The remains of the MA and all classified equipment and weapons were recovered.

Under 10 US.C. 2254(d), any opinion of the accident investigators as to the cause of, or the factors contributing to, the accident set forth in the accident investigation report may not be considered as evidence in any civil or criminal proceeding arising from an aircraft accident, nor may such information be considered an admission of liability by the United States or by any person referred to in those conclusions or statements.

MQ-IB, S/N 03-3112 17 January 2007

Figure 1.5.1 – Sample AIB Executing Summary Report

1.6. Title 14 of the Code of Federal Regulations – Aeronautics and Space (14CFR)

Before 1926, access to the national sky was completely unregulated. Because of the high incident of death amongst daredevil socialites, the aviation industry asked congress to regulate air activity(16). The public saw that regulation could improve safety and encourage growth in aviation. In 1926, congress passed the Air Commerce Act. The law established airways, standardized navigation and traffic control tools, and set a process for certifying pilots and aircraft. During the early days of regulation, the accident rate was much higher than it is today. In 1929, there were 51 incidences or about 1 accident per 10^6 passenger flight miles (17).

In the initial system, there was a conflict of interest in the certifying body, the Bureau of Air Commerce. The agency was commissioned to both promote air commerce, and, at the same time, find and publish the causes of aeronautical accidents. The agency was reluctant to admit that the accidents may have been related to their own rules and procedures. In 1935, Sen. Bronson M. Cutting was killed when his DC-2 crashed killing all aboard. The investigation of his death by congress came to a different conclusion than the investigation by the Bureau of Air Commerce. This led congress to pass the 1938 Civil Aeronautics Act. This established a new separate safety authority, the Civil Aeronautics Authority (CAA)(16).

The CAA's Air Safety Board worked independent of the Bureau of Air Commerce to conduct accident investigations and recommend corrective actions. This agency grew, and in 1940, President Franklin D. Roosevelt split the authority again into two agencies: the Civil Aeronautics Administration (CAA), and the Civil Aeronautics Board (CAB). The CAA took responsibility for air traffic control, airmen, and aircraft certification, safety enforcement, and airway development. The CAB assumed safety rulemaking, economic regulation of airlines, and accident investigation(14).

The National Air System continued to grow without legislation until 1958 when a series of mid-air incidents caused a new interest in Air Traffic Control. The NAS, at the time, had two control system, one military and one civilian. The separation of traffic knowledge was responsible for some of the mid-air collisions. The 1958 Federal Aviation Act was signed in response. This legislation consolidated the Nation Airspace into one system while assuring the military would get control of the airspace during war time. Rulemaking was transferred back into the newly created Federal Aviation Agency which replaced the CAA while the CAB focused of accident investigation(14).

In 1966, the agency was moved out of the Department of Commerce and into its own cabinet level office, the Department of Transportation. This changed it from an agency to an administration and transferred the accident investigation authority of the CAB into the National Transportation Safety Board. In 1974, the National Transportation Safety Board became completely independent of the DOT, giving us our two largest civil transportation agencies as they exist today. These organizations work in independent cooperation and mutual oversight to respond to air mishaps and transform aircraft and air traffic control into the safest mode of transportation in the country(14). As of the start of this study, the NAS has a safety rate of about 3 deaths per 10¹⁰ passenger miles, or a reduction in fatality of 3000 fold since the days of the Bureau of Air Commerce(13).

The regulations themselves have evolved along with the changes in organizational structure. Figure 1.6.1 shows a visual history of the path of regulatory change with the motivating events on the left. The first rules were called Bulletin 7 (12). The rules were informal because the Aeronautical Branch of the Department of Commerce was still only a branch of the Department of Commerce. Several of the Aeronautics Branch were dependent on

other division of the Department over which they had no authority (16). Then the Bureau of Air Commerce was created consolidating all the functions of the organization under one command structure giving the director authority over the work force involved in promoting and regulating air commerce. This is when the rules of the skies were first codified in the Civil Air Regulations (CAR). The death of Sen. Bronson M. Cutting (R-NM) in 1935 and the following discrepant cause finding of the two investigations, Congress and BAC, led to the separation of regulation of transport aircraft and small personal aircraft, CAR 4a and 4b (16). The system evolved with the introduction of Rotorcraft and the evolving separation of powers (e.g. operations, regulation, and investigation). The system of rules that exists today consists of several parts that have themselves evolved in response to new system hazards but have remained in the same hierarchy and interrelation. Figure 1.6.2 shows a list of 14CFR parts most pertinent to airworthiness certification. All product certification starts with Part 21 Certification Procedures for Products and Parts. Then the applicant is directed to the particular aircraft type for which they are seeking approval for. The main categories here are airplanes, normal and commuter category, Part 23, and transport category, Part 25, and rotorcraft, normal category, Part 27, and transport category, Part 29. These parts in turn refer the applicant to various component parts such as engine, propeller, and noise depending on the aircraft's complexity (12). In general, normal category aircraft have simpler rules that require more stout and robust airframes. This accounts for a reduced amount of design knowledge and the reduced skill and technical tools of the persons responsible for operation and inspection of these aircraft in service. Transport category which are larger and impart a larger risk on revenue providers are much more regulated, but, in return for the extra design knowledge burden, they are allowed to be more elegant and efficient aircraft that take into account the risk reduction during operation that come from higher personnel

training, and the increased environmental and conditional knowledge that is available with more sophisticated methods of aircraft and environmental observation. As an example, Part 23 normal aircraft must be able to pull 6Gs in a vertical roll while a Part 25 must only pull 2.5Gs (5). Also Part 25 aircraft in general take much more use of 14CFR 25.571(25.571) than Part 23 category aircraft take advantage of 23.573, both concern the damage tolerance of vehicles, because organizations operating Part 25 aircraft generally have a larger more equipment maintenance staff which is capable more frequent and detailed inspection of the fleet.



Figure 1.6.1 – Timeline of Agency and Rule Changes (12)

Part 1:	Definitions and Abbreviations
Part 13:	Investigative and Enforcement Procedures
Part 21:	Certification Procedures for Products and Parts
Part 23:	Airworthiness Standards: Normal, Utility, Acrobatic, and Commuter Category Airplanes
Part 25:	Airworthiness Standards: Transport Category Airplanes
Part 33:	Airworthiness Standards: Aircraft Engines
Part 34:	Fuel Venting and Exhaust Emission Requirements for Turbine Engine Powered Airplanes
Part 35:	Airworthiness Standards: Propellers
Part 39:	Airworthiness Directives
Part 43:	Maintenance, Preventive Maintenance, Rebuilding, and Alteration
Part 45:	Identification and Registration Marking
Part 47:	Aircraft Registration
Part 65:	Certification: Airmen Other Than Flight Crewmembers
Part 91:	General Operating and Flight Rules
Part 121:	Operating Requirements: Domestic, Flag, and Supplemental Operations
Part 125:	Certification and Operations: Airplanes Having a Seating Capacity of 20 or More Passengers or a Maximum Payload Capacity of 6,000 Pounds or More; and Rules Governing Persons on Board Such Aircraft
Part 135:	Operating Requirements: Commuter and On Demand Operations and Rules Governing Persons on Board Such Aircraft
Part 145:	Repair Stations
Part 183:	Representatives of the Administrator

Figure 1.6.2 – List of FAA regulations related to airworthiness certification (12)

The FAA and the rules that govern its action, 14CFR, are not static entities. The FAA and 14CFR have changed to respond to new technology, new traffic densities, and new modes of failure. They are a consolidated body of organizations and rules that have evolved to include powers such as peacetime operation of military aircraft, and tolerable mishap rates. The current

system must evolve to efficiently regulate and incorporate new classes of aircraft. 14CFR does not yet include Unmanned Air Systems. 14CFR does not currently govern the design of these vehicles, nor their operation in the NAS.

2. Methodology

2.1. Failure Mode Typology and Categorization

The first step in the assessment of the two data sets is creating a categorization scheme. The AFSC mishap summary data came in two excel files: 'VER_3.2_Auburn Expanded DataFY2000-FY2004.xls' and 'VER_3.1_Auburn Expanded DataFY2005-FY2009Product.xls'. The AFSC data, being the more complete set of mishap records, is surveyed first to come up with list of general categories that encompassed the causal mechanisms of the mishaps. These categories are broad and few in number. I conducted an initial survey to create a simple set of cause categories. This small set makes presentation of the data very accessible to a larger stakeholder audience and speed the team assessment process. This survey came up with the categories Lost Link (LL, the initial concern of the FAA that led to this study), Reduced Perception (RP), Hard Landing (HL), Reliability (RE), Maintenance Error (ME), Pilot Error (PE), and Environment (ENV) which made the independent assess of the research team produce uniform comparable results. These categories are 96% successful in categorizing the causation of these mishaps. The remaining 4% did not contain any information to facilitate categorization. These mishaps are all class E, the least severe mishap class.

A clear majority of the mishaps are shown to be caused by reliability failures. That category is divided into sub categories to give more detail into the mishap causation trends: Power Plant (PWP), Auto Pilot (AP), Electrical (EE), Hydraulic (HD), and Structural (STR).
This typology is reviewed against the AIB data with 100% classification success. The breakdown of the Reliability category gave greater fidelity to the main causal categories and allows remote and non-remote failures to be more finely separated. Remote failures are categorized as the sum of failures caused by lost link, reduced perception, hard landing, and autopilot. The remainder is considered non-remote. These failures occurred because of causes that also exist in manned aviation.

To improve objectivity and confidence, a panel of three investigators performed the categorization: an unbiased graduate mathematician, a senior aerospace analyst, and an industry airworthiness analyst. The three person panel also developed a structure to resolve differences in interpretation of the presented data. Each member went through the 240 AFSC mishap summaries and then met to compare their results. The initial categorization resulted in 90% agreement. Some areas regarding undue pilot burden and maintenance skill required debate, but, in the end, consensus was reached by the group on all mishaps.

The executive summaries for the AIB reports are created from the full unprivileged reports. The researchers took the available versions of these reports and summarized them with a focus on causation. A spreadsheet was created using data elements similar to the AFSC summary: fiscal year, model, visibility, phase of flight, summary of damage, cause summary, and damage summary. This reduced format is categorized into the same categories as above. Causal summaries that were ambiguous or led to conflicting categorizations were taken back to the original text and debated to achieve uniform categorization.

The higher level of fidelity in the AIB reports made classification of failure modes more precise than with the available SIB data. The AIB reports a qualitatively similar but quantitatively somewhat different result. That is, the same causes were identified and occurred

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in frequency at about the same order of magnitude. However, the SIB reports resulted in failure modes being assigned different percentages of the total causes. This was due to both a higher fidelity description of the event and the fact that not all of the summary AIB reports could be located. The shortage of reports degrades the breakout of the proportions for the failure rates and relegates the AIB data to being most valuable in this report as a guide for the gap analysis. Nevertheless, the breakouts of mishap rate proportions appear to be valuable for demonstrating how the complete analysis should be carried out in a follow-on effort using the complete set of full AIB reports.

2.2. Gap Analysis

The gap is focused on potential gaps between UAV experience and 14CFR which govern all other flight operations in NAS. As an example of how these gaps may be bridged, Part 25 is surveyed. First each regulation in the part is considered for its applicability to UAS. Then the current available data is exainined for its sufficiency as a Means of Compliance to the individual applicable regulations. Next, different modes of knowledge accumulation are examined for a possible testing only Means of Compliance. It was the opinion of the investigation team that DoD would be more accepting of a pure testing based certification because minimal design knowledge would be transferred into unprivileged sources. The applicable regulations are reviewed again for the sufficiency of flight and ground testing at providing Means of Compliance. Then, traditional analysis is examined as a Means of Compliance to the UAS applicable regulations. This process is very broad in nature and was done with current MALE and HALE aircraft in mind.

A more detailed look at incorporation gaps in achieved through detailed case study of the AIB executive summary. During the study of the AIB reports, more detailed common causes are

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discovered. These reports are collected and the original text of the AIB are studied in depth to look at the Gaps in airframe airworthiness. These gaps are compared to current 14CFR regulations to determine whether enforcement of current regulation would be sufficient in restoring airworthiness or if new rules need to be drafted to manage the risk from UAS introduction.

3. Failure Trends

3.1. Fleet Wide Mishap Classification

The analysis of the SIB reports resulted in the following typology of failure modes: lost link (LL), reduced perception (RP), hard landing (HL), reliability (RE), maintenance personnel error (ME), pilot error (PE), environmental (ENV), or unable to classify (==).

These categories are defined below. Lost Link (LL) is the loss of communication, command, or control to or loss of awareness information from the UA. This could be caused by lost line of sight, range exceedence, or loss of transmission capability. Reduced perception (RP) captures all elements of the operator's physical detachment from the UA and the resulting perception loss. Reduced perception is the insufficient awareness to properly react to system changes. This could be the reduction in visual resolution, view angle, and pan rate that results from fly by video dependence. Reduced perception also covers the lack of inertial and vibration forces that come from maneuvers and equipment both functioning and malfunctioning, and lack of hearing. The reaction times of an operator are also impaired by data transit speeds. When systems are in remote areas, they are guided by satellite uplink. This can impart up to a 2 sec delay between perception and action. This pushes human reaction times and creates artificial instability. Hard landing (HL), while the causes may be diverse, is simply a directed landing at above the allowed decent rate. Reliability (RE) is group of all physical failures of the UAS: electrical, mechanical, and software. Maintenance error (ME), and Pilot error (PE) divide the human factor into major interfacers with the UA. Environmental (ENV) captures all outside factors that result in vehicle mishap. This includes bird strike, gusts, storms, and reduced visibility.

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Figure 3.1.1 – Cause Mishap Frequency – All Classes – AFSC

From Figure 3.1.1, the three break away causes of mishaps are reliability, reduced perception, and hard landings. Hard landings are themselves a product of gust sensitivity, insufficient authority, and reduced perception. Reliability shows the highest incidence by 3 fold. This category is broken down in Figure 3.1.2. Most of the reliability factors appear to be controlled below a threshold of 5 per year, auto pilot and electrical being the most active controlled cause. Electrical failures could be on a delayed rise, but additional later years must be included to draw conclusions. The biggest and most divergent of the reliability failure modes is power plants. Figure 3.1.3 shows the summary break of the All Classes of Mishap break down. From the pie chart, Reliability accounts for over 50% of all UAS incidences. Also if LL, RP, HL, and AP are summed together a metric of the remote failures can be found. These sum to 47% or almost half of all UAS mishaps. This means that more than half of all UAS mishaps result from failure of systems that already exist on manned aircraft. Also, it's important to point out that pilot error only accounts for 1.2% of all mishaps. In civil aviation where equipment failures are substantially less likely, pilot error is the cause of over half of incidents. Figure 3.1.4

shows the breakdown of reliability mishaps. The dominant modes are power plant, auto pilot, and electrical, in that order. Power plant reliability is the largest single contributor of UAS incident causing 33% of all mishaps or 63% of all reliability mishaps. This is double the contribution of any other category.



Figure 3.1.2 - Reliability Cause Mishap Frequency - All Classes - AFSC



Figure 3.1.3 – Cause Mishap Breakdown – All Classes - AFSC



Figure 3.1.4 – Reliability Cause Mishap Breakdown – All Classes – AFSC

The next analysis is per vehicle type. Figure 3.1.5 shows the mishap count over time broken down by vehicle type. The majority of reported incidence occurred with the RQ-1/MQ-1 Predator. This is confirmed by Figure 3.1.7. The predator is the first, smallest and most numerous of the vehicle types covered in this study. The first trend is in the reliability of the ground control station. All drones operate from the same Multi-platform control station originally developed for the RQ-1 Predator. The first five years of operation resulted in no incidents, but towards the end of the decade, two incidents emerge. From Figure 3.1.5, it appears that mishap counts are running away exponentially for the MQ-1 and MQ-9, but, to look at future trends, the actually flight hours need to be taken into account. Figure 3.1.6 also shows an exponential growth in flight hours. Figure 3.1.7 shows the All Class incident rate of the three airframes studied. The trends appear log-linear, and the incident rate for all aircraft is reducing, even if the rate is slow. For more on rate trend analysis see Section 3.13. Most aircraft years lie between 3E-3 to 3E-4 Mishaps per flight hour. In contrast, the current tolerance of hazardous

conditions, analogous to the sum of all incidences Class B through E incidence, is 10^{-7} or 3 to 4 orders of magnitude less frequent than demonstrated.



Figure 3.1.5 – Vehicle Mishap Frequency – All Classes – AFSC



Figure 3.1.6 - Vehicle Annual Flight Hours



Figure 3.1.7 – Vehicle Mishap Rate – All Classes - AFSC



Figure 3.1.8 – Mishap Vehicle Breakdown – All Classes – AFSC

The AFSC has classification system Class A-E. Since there are no passengers, the damages, so far, have been purely financial. Table 3.1.1 explains the damage associated with each Class. Because there are no Class D Mishaps and in the authors opinion, some of the Class E would cost more than \$1000 to restore capability, some of the Class E events may be worthy

of a Class D status. The damage is approximately equally spread between Classes A, C, and E, as shown in Figure 3.1.9. This means that Class A is still within an order of magnitude of the overall mishap rate.

Class A	\$1,000,000 or More in Damages or Loss
	of Aircraft
Class B	\$200,000 to \$999,999 in Damages
Class C	\$20,000 to \$199,999 in Damages
Class D	\$1,000 to \$19,999 in Damages
Class E	Less than \$1000 in Damages

Table 3.1.1 – AFSC Damage Classification



Figure 3.1.9 – Class Mishap Frequency – AFSC



Figure 3.1.10 - Class Mishap Breakdown - AFSC

The mishap class of most importance is Class A, especially the ones that do not involve a hard landings. Figures 3.1.11 and 3.1.13 show the cause frequency temporal trends and breakdown for all AFSC Class A incidents. Reliability, the main cause of mishap, accounts for a slightly larger 57.0% of mishaps, up from 52.8% for All Classes. Lost link, one of the commissioning issues of this study, shows twice the impact on Class A incidences. What's more interesting is the porposing that shows up in the data when Class A mishaps are broken out. The reliability, power plant, and auto-pilot cause plots show smooth increases in annual frequency when All Classes are plotted, but the Class A data has a very distinct 3-4 year slow rise and sharp reaction cycle, as shown in Figure 3.1.11 and 3.1.12. In our May 17th 2011 meeting with DoD/FAA concerning this data they said the 2010 reliability numbers were "much better" adding a 3rd hump to our Class A Charts.

The next points of interest are the categories that drop out off the mix when only Class A mishaps are considered. First, all Class A mishaps are described in sufficient detail to be categorized. The typology created is 100% successful in categorizing the data. Next, looking at

the general cause data, all personnel error is removed from the breakdown shown in Figure 3.1.13., meaning besides the reduced perception of the platform, all issues are technical in nature. Moving to the reliability cause breakdown, shown in Figure 3.1.14, structural and hydraulic failures drop from the list. It is important to note that the MQ-1, which provides the most mishap data, is controlled by servos which are a source of mishap that will be talked about later in Sections 3.2 and 3.12.2. Last, while power plant, and auto-pilot failures account for the same percentage of mishaps, Figure 3.1.14 shows that electrical failures take up the complete residual of reliability failures, a 50% increase in contribution.



Figure 3.1.11 – Mishap Cause Frequency – Class A - AFSC



Figure 3.12 – Mishap Cause Frequency – Class A – AFSC



Figure 3.1.13 – Mishap Cause Breakdown – Class A - AFSC



Figure 3.1.14 – Reliability Mishap Cause Breakdown – Class A – AFSC

Figures 3.1.15-17 show trends by vehicle. The porposing trend is very distinct in the RQ-1/MQ-1 Predator Data. Surprisingly given the great range of service hours accumulated, the Class A Mishap rate falls in a tight band. These rates are also all trending downward with time. Last, the mix of vehicle mishaps is approximately unchanged at the Class A level, as shown in Figure 3.1.17.



Figure 3.1.15 - Vehicle Mishap Frequency – Class A – AFSC



Figure 3.1.16 – Vehicle Mishap Rate – Class A – AFSC



Figure 3.1.17 – Vehicle Mishap Breakdown – Class A – AFSC

The AIB executive summaries are immensely helpful in attributing detailed cause to the incidence they record, but, looking at Figure 3.1.19-3.1.20, the number of unreported incidents is very high. As an example, in 2007 thru 2009 88% percent of MQ-9 incidence went undisclosed by the AIB. In most years of this study, over 30% of the RQ-1/ MQ-1 mishaps are not reported by the AIB. As a whole, 35.4% of AFSC mishaps do not have AIB reports. The correlation of

missing reports is further hindered by the fact that the two data sets use different unique airframe identifiers. The AIB uses UAS serial numbers of 6 digits. The AFSC data set uses an RPA ID number of 3 digits. The RPA ID is not temporally or minor model sequential. This makes confidence in the causation trends, extracted from this data set as a whole, very low. However, there are things the data can show about the ambiguity of the AFSC data. There are some gross discrepancies in the data trends. Figure 3.1.24 shows the cause mishap breakdown. The first difference is in the role of personnel error. In Figure 3.1.13, there are no mishaps attributed to personnel in the AFSC Class A data, but, in Figure 3.1.24, 13.7% of AIB incidents can be attributed to personnel. This existence contradicts the AFSC data set. There are also some less firm trends that over balance the lack of reporting. The breakdown also shows a complete lack of reduced perception mishaps. Figure 3.1.25 shows the AIB break down of Reliability mishaps. The AIB data shows 300% increase in the role of Electrical Failures, 21.6% AIB over 7.6% AFSC. Count-wise the AIB is higher, 11 AIB mishaps over 6 ASFC. The meaning of the trends is undercut by the incompleteness of the AIB data set, but it is firm evidence as to the importance of follow on work to acquire the entire AIB or possible SIB reports for these incidences.



Figure 3.1.18 – Vehicle Mishap Frequency – Class A – AIB



Figure 3.1.19 – Vehicle Mishap Count Discrepancy – Class A – AIB



Figure 3.1.20 - Percent Discrepancy (AFSC-AIB/AIB) in Vehicle Mishaps - Class A



Figure 3.1.21 – Mishap Breakdown by Vehicle – Class A – AIB



Figure 3.1.22 - Cause Mishap Frequency - Class A - AIB



Figure 3.1.23 – Reliability Mishap Frequency – Class A – AIB



Figure 3.1.24 – Cause Mishap Breakdown – Class A - AIB



Figure 3.1.25 – Reliability Cause Mishap Breakdown – Class A – AIB

3.2. RQ-1/ MQ-1 Predator Mishap Classification

Because RQ-1/ MQ-1 UAS differ so much in size, payload, construction, and power plant, more precise trends can be found if these aircraft are broken out and considered individually. First examined is the RQ-1/MQ-1 Predator. This is the first UAV fielded by the DoD hence the "-1". It is the smallest UAV in this study, and the only one to have its mission changed during the production run. It is also the most popular large UAV in service. RQ-1/MQ-1 has accumulated 591,000 flight hours and 199 of the 253 mishaps reported by AFSC. The data in Figure 3.2.1 looks smooth with no cyclic patterns. Reliability is the breakaway cause for a majority of mishaps, 55.5% according to Figure 3.2.3. The largest cause of reliability mishaps is power plants, 35.2%. These rate and ratios are very similar to the total fleet data, but what is more interesting at this level is the break out of individual cause mishap rates.



Figure 3.2.1 - RQ-1/ MQ-1 - Cause Mishap Frequency - All Classes - AFSC



Figure 3.2.2 – RQ-1/ MQ-1 – Reliability Cause Mishap Frequency – All Classes – AFSC



Figure 3.2.3 – RQ-1/ MQ-1 – Cause Mishap Breakdown – All Classes – AFSC



Figure 3.2.4 – RQ-1/ MQ-1 – Reliability Cause Mishap Breakdown – All Classes – AFSC

Figures 3.2.5 and 3.2.6 show the cause and reliability cause mishap rates. All the causes start out at $1 \times 10^{-3} - 1 \times 10^{-4}$ at the beginning of the decade and decay a full order of magnitude over the decade to $1 \times 10^{-4} - 1 \times 10^{-5}$. This puts lost link in the realm of current Active Control failure limits of 10^{-5} , 14CFR 25.672. The autopilot, Figure 3.2.6, is approaching a reliability of 5 x 10^{-5} . Power Plant reliability is still at 10^{-4} , which is very far from the Hazardous Condition limit 10^{-7} .



Figure 3.2.5 - RQ-1/ MQ-1 - Cause Accrued Mishap Rate - All Classes - AFSC





Figures 3.2.7 and 3.2.8 show the cause frequencies for Class A mishaps. The porposing trend is even more pronounced in the RQ-1/ MQ-1 data than in the general fleet. Consider for example, Reliability, Power Plant, and Autopilot frequency in Figures 3.2.7 and 3.2.8. Figures 3.2.9 and 3.2.10 show no significant change in breakdown ratios.



Figure 3.2.7 – MQ-1/ RQ-1 – Cause Mishap Frequency – Class A – AFSC



Figure 3.2.8 – RQ-1/ MQ-1 – Reliability Cause Mishap Frequency – Class A – AFSC



Figure 3.2.9 - RQ-1/ MQ-1 - Cause Mishap Breakdown - Class A - AFSC



Figure 3.2.10 - RQ-1/ MQ-1 - Reliability Cause Mishap Breakdown - Class A - AFSC

Figures 3.2.11 and 3.2.12 show Class A mishap rates in the AFSC data. All the causes start out at $4 \times 10^{-4} - 4 \times 10^{-5}$ at the beginning of the decade, and decay an order of magnitude over the decade to $7 \times 10^{-5} - 2 \times 10^{-6}$. Lost link is trending towards 10^{-5} . The autopilot, as shown in Figure 3.2.12, is also approaching a reliability of 10^{-5} , both approach the failure tolerance for active controls. If autopilot is developed to have acceptable sense and avoid, the system will

required a double fault to produce a mishap. This means a mishap rate of 10^{-10} which actually meets the current catastrophic mishap tolerance of 10^{-9} , hypothetical, but promising.



Figure 3.2.11 - RQ-1/MQ-1 - Causation Accrued Mishap Rate - Class A - AFSC





The trends shown in Figures 3.2.13 through 3.2.16 are almost identical to those shown in Figures 3.1.21 through 3.1.24. The reactionary porposing shown in the AFSC data is indiscernible. Auto Pilot accounts for a larger fraction.



Figure 3.2.13 - RQ-1/ MQ-1 - Cause Mishap Frequency - Class A - AIB



Figure 3.2.14 – RQ-1/MQ-1 – Reliability Cause Mishap Frequency – Class A – AIB



Figure 3.2.15 - RQ-1/ MQ-1 - Cause Mishap Breakdown - Class A - AIB



Figure 3.2.16 - RQ-1/ MQ-1 - Reliability Cause Mishap Breakdown - Class A - AIB

3.3. MQ-9 Reaper Mishap Classification

The MQ-9 Reaper, also called the Predator, is the second generation MALE UAS from General Atomics. The maturity of the platform design can be seen in the breakdown of mishaps, even if the annual mishap rate does not reflect this. Figure 3.3.1 shows that reliability does not become an issue in the airframe until 4 years after entry into service. The main causes of mishap during the first 4 years are hard landings and reduced perception. These are both remote failures. Looking at Figure 3.3.2 another mature trend arises. The electrical failures follow the mechanical ones. In general, reliability plays a much smaller role, 35.3%, in causing mishaps, as shown in Figure 3.3.3. However, inside reliability power plants account for 72.7% of reliability mishaps, or 23.5% overall contribution. Also of note, no personnel mistakes appear to have contributed to mishaps. Without more data no additional conclusions can't be made from that fact.



Figure 3.3.1 – MQ-9 Cause Frequency – All Classes - AFSC



Figure 3.3.2 – MQ-9 Reliability Cause Frequency – All Classes – AFSC



Figure 3.3.3 – MQ-9 Cause Mishap Breakdown – All Classes - AFSC



Figure 3.3.4 – MQ-9 Reliability Cause Mishap Breakdown – All Classes – AFSC

The MQ-9 has only accumulated 50,000 hours so it is still early in its development curve and still has a lot of maturing to do. The hard landing mishap rate is significantly higher than the current MQ-1 rate. It's still 4 x 10^{-4} at the end of the decade, and compare that to start of the study, 3 x 10^{-3} . The rest of the causes are still 10^{-4} , which is 3 to 4 orders of magnitude higher than transport aircraft.



Figure 3.3.5 – MQ-9 Cause Mishap Rate – All Classes - AFSC



Figure 3.3.6 - MQ-9 Reliability Cause Rate - All Classes - AFSC

For Class A mishaps, the causation becomes very simple. There is only one type of reliability that has caused a vehicle loss, power plant as shown in Figure 3.3.8. As show in the All Class data, remote failures dominate the mishap causes, as shown in Figures 3.3.7 and 3.3.8. Remote failures account for 80% of MQ-9 mishaps. Figure 3.3.9 shows the accrued mishap rate. The figure shows that there are only a few data points to go by, but one trend that appears to be different is the hard landing rate. The hard landing rate has almost no downward slope.



 $Figure \ 3.3.7-MQ-9-Causation \ Mishap \ Frequency-Class \ A-AFSC$



Figure 3.3.8 – MQ-9 – Causation Mishap Breakdown – Class A – AFSC



Figure 3.3.9 - MQ-9 - Causation Mishap Rate - Class A - AFSC

The AIB data, shown in Figures3.3.10 and 3.3.11, are included only to show the lack of inference that can be made from 2 data points when 8 points are missing from the record.



Figure 3.3.10 - MQ-9 - Cause Mishap Frequency - Class A - AIB



Figure 3.3.11 – MQ-9 – Cause Mishap Breakdown – Class A – AIB
3.4. RQ-4 Global Hawk Mishap Rate

The RQ-4 shows very similar trends as the MQ-1 even as the number of mishaps and flight hours does not give the fidelity to see growth. The RQ-4 is the largest and most expensive drone in this study. The level of reduced perception shown in these figures is questionable because the AFSC and AIB data disagree, more in the RQ-4 AIB discussion. The RQ-4 also implemented auto-landing navigation, which can be seen in the lack of Hard Landings, as shown in Figures 3.4.1 and 3.4.2. Power plant reliability is still a major issue in this platform accounting for 35.3% of all Rq-4 mishaps, as shown in Figures 3.4.3.



Figure 3.4.1 – RQ-4 – Cause Mishap Frequency – All Classes – AFSC



Figure 3.4.2 – RQ-4 – Reliability Cause Mishap Frequency – All Classes – AFSC



Figure 3.4.3 - RQ-4 - Cause Mishap Breakdown - All Classes - AFSC



Figure 3.4.4 – RQ-4 – Reliability Cause Mishap Breakdown – All Classes – AFSC

Because of the extremely low flight hours and early unreliability, the RQ-4 started service with a horrible crash record Figures 3.4.3 and 3.4.4. The end year rates are comparable to the RQ-1 performance; however, the slopes are more dramatic. This suggests a faster rate of improvement.



Figure 3.4.5 - RQ-4 - Cause Accrued Mishap Rate - All Classes - AFSC



Figure 3.4.6 - RQ-4 - Reliability Cause Accrued Mishap Rate - All Classes - AFSC

According to the AFSC data, reduced perception is the main cause of Class RQ-4 mishap, Figures 3.4.7 and 3.4.8, accounting for 75% of lost aircraft. The rate of incident is comparable to the other aircraft.



Figure 3.4.7 - RQ-4 - Cause Mishap Rate - Class A - AFSC



Figure 3.4.8 - RQ-4 - Cause Mishap Breakdown - Class A - AFSC



Figure 3.4.8 – RQ-4 – Cause Mishap Rate – Class A – AFSC

The AIB data here, while incomplete, shows a different story than the AFSC data. The three mishaps match up exactly with the times of the first three AFSC data, but the cause determination is different. In 2000, the AFSC data brought the determination reduced perception while the AIB report brought the determination autopilot failure. Likewise, the 2002 reduced perception mishap is determined to a structural reliability issue.



Figure 3.4.9 - RQ-4 - Cause Mishap Frequency - Class A - AIB



Figure 3.4.10 - RQ-4 - Reliability Cause Mishap Frequency - Class A - AIB



Figure 3.4.11 – RQ-4 – Cause Mishap Breakdown – Class A - AIB



Figure 3.4.12 – RQ-4 – Reliability Mishap Breakdown – Class A – AIB

3.5. Causal Trends

While the AFSC data is a more complete data set and can be used to determine the number of incidents that occurred, the SIB one-line summaries lacked the detail to give any further insight into the exact cause of the incident so more detailed trends could be discovered. This section looks at the AIB reports in detail and common causes found.

3.5.1. Power Plant

Power plant system failures accounted for the largest fraction of mishaps and catastrophic incidents. Looking deeper into the cause of failure in this system reveals a wide variety of causes. Broadly, mishaps occurred from both mechanical and electrical causes. There is evidence of poor initial quality. On17 Jan 07, a MQ-1B crash occurred from initial manufactured quality of the crankshaft which cascaded into full engine seizure. On 19 Nov 09, a MQ-1B crashed because the quill shaft had been improperly quenched during heat treatment. These cracks lead to early fatigue failure of the variable pitch prop mechanism. On 30 Jun 07, the MQ-1B crashed from improper soldering of the Ignition Module. This redundant system was not designed to fail safe. The excessive heat due improper enclosures design and the intolerance of the second ignition system to over flow current from the first system's failure proves the system is not designed to fail safe, and the second system was an insufficient back-up. If the ignition system was held to 33.37 and 33.28.d.3 and f, this would not have occurred. As well as design and construction of materials 25.603 and 25.619.

Determinate assembly and routing is another issue that pervades over power plant failure. 5 MQ-1 were lost from systems that were not designed with determinate assembly. When taken apart they could be put back in more than one way, and no marking were given to prevent that. On 20 March 09, a mishap was caused by an improperly assembled oil temperature control

valve. In three other cases, mishap was cause by the mechanics routing fuel, oil, and vacuum lines in a way the original designer had not thought about, in most cases, draping the line over the exhaust manifold. The other systemic cause of failure in the MQ-1 power plant is the Variable Pitch Prop Mechanism.

This Variable Pitch Prop Mechanism of the RQ-1/ MQ-1mechanism itself has several vulernerable modes of failure. Failure of this single mechanism has caused 6 Class A incidents totaling \$24 million in losses. The mechanisms failure history is a good case study for UAS as a whole. The failures have come from both mechanical and electrical sources. The electrical failures of this system were centered in the improper manufacture of the servo motors, and the mechanical failures centered around the quill shaft that directly controlled propeller pitch and the bearing isolating this shaft from propeller rotation. The failure of this mechanism, while small, lead to unforeseen consequences in larger system. Below are two example exerts from AIB reports three years apart: 30 March 2005 and 19 Oct 2009.

"There is clear and convincing evidence that this mishap was caused by the failure of the pilot bearing that encases the variable pitch propeller quill shaft. Damage analysis of the pilot bearing and quill shaft suggests a long duration, progressive failure within the unit. The failed pilot bearing, which is supposed to allow the propeller shaft to spin freely around the fixed quill shaft, caused enough friction to torsionally sheer the adapter which holds the quill shaft in place. The engine anomaly occurred during the initial sheering action as heavy drag was being placed on the engine via the propeller shaft. Once the adapter sheered, the quill shaft then unscrewed itself from the variable pitch propeller servo and drove the propellers to a negative pitch setting causing severe drag and high sink rates."

"The Accident Investigation Board President found by clear and convincing evidence that the cause of the mishap was the failure of the quill shaft bearing which caused the variable pitch propeller quill shaft to engage and then turn with the propeller shaft, dramatically and uncorrectably altering the pitch of the propeller blades which impacted engine performance and thrust setting at an extremely low altitude and made the aircraft unrecoverable. The bearing failure was attributed to the use of a bearing installation tool worn and used beyond the designed specifications which damaged the roller bearing case during installation."

In both incidences, the pilot bearing seized shearing the quill shaft causing the shaft to unscrew itself from the servo. This pushed the propeller to a negative pitch angle creating negative thrust. This slowed the aircraft to an unrecoverable speed. This also had another unintended consequence. Because of the power plant orientation and packaging, the reversal of air across the engine caused a starvation of the intake. This caused the engine to bog down and lose power.

Because the exact crash details are unknown in the summary level details of the AIB executive summaries, absolute confidence in cause is not available in the current information. Instead a list a possible causes is developed, and verification testing suggested to prove causation.

The first cause could be loading outside the design envelope. The propeller passes very close to the lower control surfaces. This buffeting could cause super cycling of the mechanism covered in 25.251, or super cycling could be the result of internal aeroelastics. Either way this could be tested with standard whirl flutter testing, varying environment and operation to cover the design flight envelope. The environment and usage could also have higher variation than the original design to cause high cycles failure. Long term instrumented monitoring of fleet would provide sufficient data to confirm environmental and operational envelope.

The other cause could be simply inferior part or maintenance procedure. This would indicate that the original design flight loads are sufficient to a produce an airworthy part, but part or procedure do not fulfill or sustain part function. To test this theory would be less expensive because it could be done on the ground with a sub-assembly. If the part fails under the original

design load envelope, inferior part or procedure is the cause. It is interesting to note, in the reports the 200 hr rebuild of this component is mentioned several times. AC 35.42 says propeller components should withstand cyclic loading for a minimum of 1000hr without maintenance.

Either way, this failure should prohibit continued flight. 25.933b says specifically that one fault should not result in the reversal of thrust. If the fault would only result in some minimum flight regime setting sufficient to sustain continued flight all the way home, the fault would only be a hazardous flight condition which 100x more tolerable.

3.5.2. Lost Link

The UAS in this study have two forms of remote awareness, command, and control: a Ku band Satellite link and a direct line of sight RF connection. The link to and from the UAS are separate and can fail separately. While only 8% of the mishaps in the AIB reports are considered caused by lost link, 15 of the 51 or 29% AIB mishaps summaries report a loss of link during terminal operation. Some are system faults; some come from the limited view angle of the transmission devices; some are cause by the speed of the maneuver. If UAS are to be allowed in the NAS, their connection to pilot should be at least 10^{-5} , the same as existing active control standards, 25.672. Also, this connectivity cannot be maneuver dependant. During active maneuver is when connectivity is most important. In addition, for lost link to be a tolerated inconvenience rather than a threat to Air Safety, the command link need must be re-established automatically. In some cases it was impossible to reestablish command connection. A few of the UAS were able to regain video and telemetry but were never able to regain command. If reliability and reconnectivity are improved, the reliability of this system does not have to approach 10⁻⁹. That level connectivity is out of the reach of current communication technology and network coverage. Last, the speed of the link is an important factor in UAS stability. When

the system is controlled via satellite link, the delay time from command to maneuver to video and telemetry confirmation can be as long as 2 secs. In a few incidences, the UAS enters a violent porposing. This is initiated by a maneuver and causes the UAS to oscillate divergently because of feedback delay until link is lost, and the UAS is destroyed.

3.5.3. Auto Pilot

In order for lost link to be a manageable issue, auto pilots must be a reliable back up to direct control. To start, this means that the programming should be thoroughly tested. On 11 Dec 03 an RQ-1L was lost because the software connection set the pitch stick 9 degrees high without notifying the mishap pilot. On 14 Sep 00, the pilot was able to dump the RAM of the Primary Control Module with a single unintelligent trigger pull. Also, as stated earlier, the AP needs code to attempt Ground Control System reconnect from its end.

The next comments involve the capability and knowledge of the Auto Pilot control. The current auto-pilot is completely unaware of its surrounding. UAS knows position and altitude, but in a few cases when the UAS went to Lost Link profile it did not maintain the proper altitude. Also in this autonomous state, the aircraft is unaware of weather or terrain (i.e. mountains). While current sense and avoid attempts to guide UAS well clear of uncooperative aircraft, these systems are not currently successful. The capability to see weather and large static terrain features already exists. If Large UAS incorporated these capabilities at least 6 of the UAS in this study could have survived their Lost Link conditions. The last comment is about design knowledge of vehicles limits and dynamic response of wings. On 30 Mar 01, a RQ-1L pitot heater was left off causing the pitot tube to ice over. The pilot turned the pitot tube heater on to alleviate the problem. When the blockage melted off, the plane violently pitched up to restore altitude. This buckled and detached the left wing. The long flexible wings of these aircraft make

dynamic prediction more difficult but not impossible. The limit strength of these UAS are known quantities. While a pilot should have the authority to overpower deterrents and rip the wings off in an attempt to save the craft and people on the ground, autopilots should not have this authority, and the internal mass models should be of sufficient fidelity to know dynamic position.

3.5.4. Hard Landing / Reduced Perception

One interesting indication of the reduced perception is seen in the Class E environmental mishaps. A large number of these incidences are bird strikes, something pilots would usually avoid at these speeds. Reduced perception is the "inherent design flaw" of a remotely operated platform. Remote command takes from the pilot the ability to "fly by the seat of his pants". UAS are much more dependent on the ability to feel than originally thought. The GCS offers no G-forces, no vibrational feedback. This positive and negative feedback give the pilot operational confidence. Vibration and auditory feedback eases the burden of situational awareness. On 26 Mar 07, a MQ-1B crashed during landing because the pilots attitude and position reference was lost during landing approach. The following passage shows how flying by video limits field of vision and takes away scale sensitivity.

There is clear and convincing evidence the mishap was caused by pilot error. The mishap pilot (MP) misjudged the RPA height above touchdown and confused the initial bounce with a normal aircraft response to his flare inputs. This confusion resulted in the MP setting a neutral pitch input with the erroneous perception that such an input would hold the attitude observed during the bounce. Instead, the neutral pitch input commanded the aircraft to return to its previously trimmed state. As commanded, the aircraft returned to approximately 4-degrees nose low and impacted the runway. Following the subsequent bounce, the MP initiated a go-around; however, he failed to provide the necessary pitch input to establish the go-around attitude. Instead of commanding a nose high pitch attitude, the actual pitch inputs commanded the aircraft nose low on each subsequent bounce. There is clear and convincing evidence that the aircraft hit the runway nose low on the fourth bounce with sufficient velocity to break the gear, and the fifth bounce damaged the multi-spectral targeting system beyond repair. Substantially contributing factors to the mishap are the lack of visual cues and the lack of cues to provide perception of body position and movement in the ground control station. The unique flight control logic and lack of pilot feedback also substantially contributed to this mishap. The lack of cues is part an inherent design flaw making the system conducive to the types of perceptual errors that occurred during the mishap sequence. These perceptual errors, unique flight control logic, and lack of pilot feedback combined to create a situation in which the aircrew was unable to recognize the proper control inputs necessary to effect recovery.

While there is no practical way to re-insert the full fidelity of the G-forces and vibrations back into the Ground station, there are some senses that can be added back. None of the UAS in this study have on board audio. On board audio would give the ability to broadly monitor on board health. Onset of noise can be a sign of impending equipment failure, as well as the end of an expected operational noises. Reduced perception will always be a part of UAS operation. It will dictate the requirement of auto-pilot systems, but awareness can be created to safely operate UAS beyond line of sight.

3.5.5. Improper Envelope Review

This is an example of haste in rapid development and deployment of technologies. The RQ-1 was originally designed as an intelligence, surveillance, and reconnaissance drone. The entire payload is stored internally. The CG envelope is expanded with the addition of two hell fire missiles weighing approximately 110 lbs each. The aircraft is completely capable of operation with the extra weight, but the CG envelope was expanded without proper investigation of the expansion in conjunction with the variation of operational environment. When one missile is fired, a static moment is left from the single missiles imbalance. This is tolerable when the air

is still, but when the aircraft is in cross wind gusts of sufficient strength the asymmetry of roll authority can be too much to handle. The aircraft goes into an unrecoverable spin. Payload and aircraft CG's need to analyzed across environmental and operational conditions before they are deemed airworthy. This means varying winds, temperatures, and densities. This also means examining the effect of single point failures, like variable pitch prop mechanisms, control surfaces, available horsepower, and control delay.

3.5.6. Residual Control and Other Design for Robustness

One theme that pervades this study is the effect of single point failures. 14CFR being a reactionary set of rules has robustness built in to it. A single bearing in the variable pitch prop mechanism should not cause a reversal of thrust. On the same note, the lower control surface failures should not result in a system fatality. Four MQ-1 are lost from insufficient control after a tail control surface malfunctioned. These aircraft are too valuable, and the risk to the domestic public is too high to be intolerant of single point failures. This system is also poorly designed because it also suffers from determinate assembly issues. If these systems cannot fail safe, 14cfr has other concept of reliability that can be practiced.

For hard quench parts like the quill-shafts which for this example cannot be made redundant and which operate in high cycle environments, Safe-Life is the proper method of certification. This means that the operational environment is understood well through conservative testing. A life span is created with proper severity and duration. Then the part is tested to a multiple of this duration to show compliance, say 3 times the expected service life. Once certified, the parts are allowed to be used for the designated Safe-Life, after which they must be replaced or inspected to a level of detail to insure no cracks have formed in the part

surface. Techniques such as Magnetic Particle Inspection and Dye Penetrant Inspection are very sensitive to surface flaws and can guarantee the part is starting over in an as-new condition.

A single control surface failure should not compromise the control of the aircraft, or that failure should be made extremely improbable. With proper design, residual control of a fault tolerant system could be a more cost effective solution. Residual control is a necessity especially for a combat vehicle but also civil UAS. This residual control should be satisfactory without requiring exceptional skill, either, because these systems need be usable by the general population if the UAS system is to grow.

3.6. Predicted Mishap Rate and Rate Trends

Figure 3.6.1 shows how maturity has progressed in each model. Rather than showing the accrued mishap rate vs. year, this figure shows accrued mishap rate vs. accrued flight hour. While still in a tight band, it shows the MQ-1, the first UAS in service, has a higher rate of incident than the later programs. Figure 3.6.1 also shows the RQ-4, the most expensive and airplane like in construction to be making a much steeper improvement in mishap rate.



Figure 3.6.1 – Vehicle Accrued Mishap Rate vs Accrued Flight Hours – Classes A – AFSC

Figure 3.6.2 shows the Class B-E incidents i.e. the non-catastrophic incidents. These incidents are ones that could be tolerated as hazardous conditions because they are not catastrophic. The interesting trend here is how tight and flat all the curves are. Figure 3.6.3 uses essentially the same parameter. Here the Log10 of the mishap rate is plotted to ease data trending. Each vehicle is modeled using a linear regression. The MQ-9 first data year 2003 is removed as an outlier. The results are interesting. First, in Figure 3.6.3, the RQ-4 has a very slight positive slope on the rate of hazardous incidents. The mishap trend can at least be called flat. This means something must be done, priority wise, to implement lower level corrective actions before these hazardous mishaps can come down to tolerable levels. The MQ-9 can also be considered flat since it won't reach tolerable levels for over 200 years. The RQ-1 / MQ-1 is the only vehicle that will meet levels in this century, but do to the short time span of this study, all UAS have an approximately flat trend in their rate of hazardous mishaps.



Figure 3.6.2 – Vehicle Accrued Mishap Rate– Classes B-E – AFSC



Figure 3.6.3 – Vehicle Mishap Rate w/ Forecast – Classes B-E – AFSC

Figure 3.6.4 shows the rate of catastrophic incident in UAS. These curve have a much more deliberate downward slope. The log10 of these values is plotted in Figure 3.6.5. The linear regression of this is much more reliable. The lowest R² is 0.86 which is the MQ-9. The RQ-4 like shown in Figure 3.6.1 will achieve certifiable crash rate in 30 yrs. This is substantially after the 2015 deadline imposed by the 2012 FAA reauthorization (10). Even this trend is extrapolated to far, but the point is made that the rate of incident reduction is very slow and very far from acceptable rates for aircraft currently certified to fly in the National Airspace System, NAS.



Figure 3.6.4 – Vehicle Accrued Mishap Rate – Class A – AFSC



Figure 3.6.5 - Log(Vehicle Accrued Mishap Rate) w/ Forecast - Class A - AFSC

4. FAR for UAV

4.1. Current Standards

4.1.1. Part 23 – Agricultural Aircraft

Agriculture aircraft certification is based on the historical Part 8 of the Civil Air Regulations (CAR). Under this Part, the applicant for a new aircraft is required to show compliance with all of the airworthiness requirements of any other aircraft category prescribed by the CAR, except those requirements which the Administrator finds inappropriate for the special purpose for which the aircraft is to be used. In addition, the applicant is required to show that the aircraft has no unsafe features or characteristics that would render the aircraft unsafe when operated under its prescribed limits. The preamble for Part 8 states that for such restricted operations where public safety is not endangered, it appears unreasonable to require the same level of safety as that required for passenger carrying aircraft. The intent of Part 8 was to place the minimum possible burden consistent with public safety on the applicant for a type certificate in the restricted category (20). A recommended list of these inappropriate requirements is contained in Appendix 1 of AC 21.25(20). The appendix covers Flight, Structure, Design and Construction, and Equipment. A long list of certification requirements are waved: high speed characteristics, pressurization, flutter, trim system, emergency exits, ventilation, seatbelts, oxygen systems, navigation instruments, power plant instruments, ditching equipment, and ice protection. None of this is required to be aboard an agricultural aircraft, even the seat belts. Allowing land owner and pilot to be solely responsible for operations and liability. UAV certification could take this form allowing the applicant to create a list or the administration to recommend a list of type certificate elements they find inappropriate for safe operation in the NAS.

4.1.2. Airship Model for Certification and Operations

Some at the FAA suggest that UAS certification and operation be based on an airship model. The definition of an airship is an engine-driven, lighter than air aircraft, that can be steered (19). This definition means there are several aspects of airship operation and construction that do not apply to heavier than air craft and several aspects of airworthiness not covered by existing rules.

Airships, being large, slow vehicles, do not have the same concept of stability, and environmental or authoritative. The stall requirements are insufficient for UAS design because they do not address minimum controllable speed, envelope coverage of stall, or recovery from stall. The authorities needed in an airship are different during landing and balked landing. The slow speed of airships precluded Go-Around required climb rates necessary in high speed aircraft. The amount of authority required and the speed of its application would be insufficient for UAS. The required nominal climb rate for airships is vertical speed based where for other aircraft it is trajectory based, gradient of climb. Based on vehicle speed the airship climb rate maybe impossible or insufficient depending on the aircraft. Landing in general is a different operation for airships. Airships can land gracefully without engines, and loiter indefinitely until they find a suitable spot. Airships are required to restore level flight after loss of all engines. How would a UAS do this? Heavier than air craft are more dependant on their power plants. Wheels, tires, and brakes have a different function for airships. Airplane rules require acceleration-stop criteria that allow for last minute abort if engines fail on take-off. These rejected take-off loads are very severe. There are more, but it is sufficient to say airships and aircraft are different type classes for a reason. Last, airship rules do not handle the high-tech navigation, auto-pilot, and control systems required by UAS. The list of rules may be shorter for

airship, but they do not sufficiently capture the necessary operations of heavier than air craft. Nor the hardening of systems for its dependency. This why AC21.17-1A "TYPE CERTIFICATION—AIRSHIPS" says the following:

" (1) In the event that the airworthiness criteria prescribed in the ADC[18] are inadequate or otherwise inappropriate as a certification basis of an airship due to its unique design or design features, other criteria may be developed. FAA approval is required before the initial application of the airworthiness criteria as the certification basis of an airship." (19)

"(3) Previously approved airworthiness criteria, when proposed for a new project, should be evaluated for currency based upon advancement of the state-of-the-art airship design, service experience, and amendments to appropriate regulations, such as parts 23 and 25 of the FAR." (19)

The operational right of way of airships also does not apply to UAS operation in the NAS. Airships are huge and slow. They have high visibilities by other craft and comparatively small speed and maneuver authority. 14CFR 91.113.d.3 says "An airship has the right-of-way over a powered parachute, weight-shift-control aircraft, airplane, or rotorcraft." This will be dangerous if applied to UAS. The visibility is much lower by other craft and the cruise speed and control authority are substantially higher. Powered parachutes, and weight-shift-control aircraft will not have the authority to dodge these craft. The fact that UAV's can't see these craft in return is cause for more sensitive sense and avoid equipment mandates, not airspace right of way.

This is why the UAS cert basis stated here uses a heavily pared down version of Part25 that allows for heavy substitution of analytic proof under a total Secondary Structure classification.

4.1.3. Part 25 – Transport Category

The large UAS of interest in the study are all operated by the DoD. UAS are flown by well trained pilots from standard bearing flight schools. They are repaired by certified airmen of best in class skill using enhancing inspection techniques. These UAS have robust maintenance programs that track system faults and incorporate mishap investigation findings into their maintenance and operations procedures. These aircraft will have state of the art environmental and operational awareness equipment, TCAS III, and advance autopilots capable of acting on this information. The HALE and MALE aircraft are elegant and thin. Long endurance systems do not make severe maneuvers and with sufficient AP limitations would not impart excessive loads on to the airframe. Transport category aircraft already have complex navigation that interfaces with other systems. The flutter requirements already incorporate guidance for failures of active stability systems. Part 25 has requirements for fire resistant and hardened electrical and controls systems, and incorporate fly by wire. All UAS in this study use fly by wireless command distribution. The aircraft, in general, are more elegantly designed and critically margined like large UAS. The increased knowledge and operations training allows these aircraft to be certified to lower loads than Part 23 aircraft, setting a more detailed but lower maneuverability and capability bar. For these reasons, Part 25 would be a better choice as a base line for UAS certification.

Part 25 rules are the best starting point for UAS certification, but these aircraft standards also have regulations that are inapplicable to passenger-less aircraft. The high standards are necessary for such sophisticated and elegant aircraft, but the compliance burden can be made less severe. Using the Agricultural model, Part 25 is review for individual rule applicability. The remaining rule set could provide a cert basis for 14CFR UAS Type certification.

Part 25 also has a huge proof burden that involves hundreds of hours of actual demonstration of airworthiness. The space coverage for a UAS is not as critical because of the lack of immediate passengers. If the entire vehicle is treated as secondary structure, the necessarily detailed standards of Part 25 could be met solely through written proof of quality of construction, controllability, sufficiency of design loads, and proof of structure under those loads.

4.2. Applicable Rules

Review of Part 25 for UAS cert basis took sustained controlled flight, structural integrity, and controlled ditching as the main priority for UAS operation in the NAS. The UA must stay in one piece, even in inoperable conditions, so the ground risk is local and infrequent. Also, the UAS must be controlled right to the moment of impact, so that its risk can be minimized from ditching. There is still no crew aboard, and if the individual systems can be hardened to tolerate neighboring failures, such as fire, there is no need for some internal safety equipment. Appendix A of this document contains the detailed examination of each rule. Out of the 397 rules in Part 25, 282, or 71% of rules are found applicable to UAS.

This means 29% or 115 rules can be ignored. The largest categories of omitted rules involve water landings, cabin safety, emergency equipment, ditching, and fire protection.

The general safety of the interior is not an issue. General requirements for accessibility, sharp edges, and ventilation are no longer necessary, but, due to the reduced size, alternate form of inspection are needed to observe the remote interior crevices in these systems. Fire safety can be considered in a different light for UAS as well. A hot structures ideology could be beneficial for UAS. As long as primary structure and systems are fire hardened, suppression systems are no longer required. The system must be sound, not comfortable.

ETOP requirement for long flights over water require extra knowledge about engine reliability and engine characteristics that are not necessary for UAS. Nor is the integrity and grace of its entrance into the water a safety concern.

This study concluded that Landing and Landing Gear rules should still apply to UAS, but these rules could be considered inapplicable under certain restrictions. These rules are retained because of the possible collateral damage of the UA skidding off uncontrolled, but this action depending on the size of the UA could be committed without any risk to other parties. The severity of the impact and the ability of the aircraft to sustain such impact are purely financial in nature, as long as fuel is still contained. The burden for malfunction would solely be on the manufacturer and operator and not necessarily create liability to any other parties. Since the main purpose of 14CFR is to protect innocent non-consenting parties, the argument could be made that certain systems are not necessary because they only provide financial risk to the risk takers themselves. Structurally UAS are, to date, much simpler vehicles. They have no high lift devices or speed brakes. For that reason, lift and drag devices are not included in this list. Also taking into account ground incident rates and physical vehicle size, acceptable safety rates to protect the public can be achieved without backup/dual control systems. This would allow UAS to be a flying test bed to improve the reliability of manned control systems.

This UAS Type Certificate(TC) is a restricted Class TC. Part of the restrictions of this certificate would include Balanced Field Length extensions, weather avoidance criteria, and daytime only operation. These operational restrictions would preclude the necessity for certain design features. The proof of these structures should also be modified as stated above to make the entire vehicle secondary structure, which would severely reduce the test burden and open up the reach of analytical substantiation based on historical and more fundamental data.

In reviewing 14CFR, one aspect of UAV operations that is wholly new to the certification plan is the issue of lost link. With the pilot removed from the aircraft, some method of wireless communication must be used to connect the pilot to the primary control system and onboard systems back to pilot. Creating a confident link that maintains the existing reliability of a pilot's physical connectivity in a manned aircraft may be outside the capabilities of current network technologies. Rather than designing in, and relying on, extreme improbability of a link failing, a lost link system should be considered as an active control with a new state of the art autopilot that provides confident residual control. This allows 10⁴x more faults in either system.

5. Compliance

5.1. Applicability of Existing Operational Data

The existing data reviewed in this research is considered as an alternative means of compliance to Part 25. However, the data submitted to date is a list of mishaps. The rate of failure documented to date is still too high to show compliance for most systems mentioned in these reports; however, there are some rules that could be shown compliant by this evidence. The UAS has successfully sustained seven bird strikes from the AFSC data. The details of these SIB reports could be used in substitute of part of the verification testing and analysis required, but a systematic coverage of the flight and control structures is needed. Also, analysis would be required to extrapolate the impact worthiness of unhit edges. Each incidents would have to be examined for the extent of satisfaction of current test standards. The number of structural failures is very low in these UAS. This could eventually be used to support Proof of Structure. The accumulated flight hours by fleet leaders could be used as proof of fatigue resistance, but the quantity of flight hours available is still insufficiently small. These are only 3 of out of 282 required rules that can be shown partially compliant through the existing data gathered in its current form.

5.2. Fleet Observation

For operational flight hours to be useful in certification, the incidence and the severity of the survived flight damage must be known, not merely a list of fatal defects. This would require some form of acceleration and/or strain data to capture the variation of the operating environment and the typical usage envelope. Once a conservative multiple of the desired cert life damage has been attained by the experimental fleet and fleet leaders, a conservative operational envelope can be derived from the data and applied to new members of the fleet,

perhaps for usage in more populated airspace. Aircraft operating in this observed envelope would be fatigue airworthy for the observed service life. This experimental operational envelope would not necessarily be required to have a basis in the envelope of an aircraft's physical limits except for the fact the operational envelope must be conservative to the physical limits and must address comprehensively the expected certified operating conditions. Damage Tolerance can also potentially be partially addressed by this method, but additional knowledge about the quality of construction and initial flaw sizes would be necessary. Sensored fleet observation data could also be an excellent source for maximum gust and pilot ultimate maneuvers data for use in setting operational limits and exceedance inspections. Some unmanned systems are substantially smaller than the manned vehicles that operate in the same environment. The smaller size raises the area to mass ratio of the vehicle causing increased acceleration due to similar gust strengths. Long term fleet monitoring would provide substantially more data to derive more accurate gust acceleration spectrums. Existing regulations should be reviewed against this spectrum data to ensure the current rules contain the minimum maneuverability and stability necessary for these potentially more environmentally sensitive vehicles to operate safely. Long term data acquisition on an existing fleet could likely produce sufficient event experiences to meet some control and integrity requirements without a need to determine the maximum capabilities of the vehicle. This would reduce the amount of dedicated test vehicles and test time necessary to certify UAS in the areas addressable by fleet data. This type broad based observation would also provide superior coverage of manufacturing variation.

5.3. Flight and Ground Testing

Most applicable regulations will not be addressed by fleet experience alone because they involve combinations of severe maneuvers with environmental extremes or operational malfunction. Most regulations are meant to ensure sufficient capability in critical situations. These ultimate capabilities are more addressable by tailored tests designed to take the aircraft to the edges of its required capability.

As an alternative to analytic substantiation of an experimental fleet, a larger set of flight tests, ground tests, and inspections can be performed to validate a wide range of capability requirements in an existing fleet: electrical, structural, control, stability, accessibility, and operation. The applicable regulations were reviewed to isolate those in which design and regulatory knowledge could be used to develop definitive tests whose passage would demonstrate regulatory compliance. With sufficient design knowledge, it was found that a majority of the applicable regulations could be addressed by a combination of pass/fail flight test, ground test, and inspection that would divulge minimal platform capability to public record. The UAS will need substantially more sensors to verify the structural airworthiness of every component of the assembled aircraft by this method. Traditionally, flight tests are used to verify the accuracy of maneuver load predictions, and structural substantiation is done analytically to capture manufacturing and environmental variation. However, a sufficient test fleet size would provide superior coverage of manufacturing variation, but the number of required tested will be a high multiple of the analysis backed test plan necessary to prove compliance across the full environmental/operational space. A safe pure testing based cert also will have to have built in it extra conservatism that accounts for the inability to locally address local knock-down factors,

like casting and fitting factors. Instead, test loads will have to be amplified by these modification factors to insure their conservative inclusion.

The review in Appendix A of this document shows these method of flight and ground testing would cover a large majority of requirements, 94%, making it a viable option for a reduced analysis certification.

5.4. Analytic Compliance

The traditional use of substantial analysis verified by minimal testing provides a very efficient means of compliance that can use existing variational data and allows future expansion of the aircrafts capability to be based on previous model data. A pure testing based approach would be more pass/fail in nature, and knowledge of the vehicles reaction is much lower fidelity without analytical extrapolation. This data would be more difficult to apply to future models without a large volume of supporting analysis. However, in some cases, analytical proof is expensive and requires a larger body of expertise than a more testing based approach; therefore, UAS certification rules should accommodate tradeoffs between these two means of compliance.

Analysis is a tremendous saver of resources. Analytical interpolation and extrapolation allows you to apply historical and variational data to the current problem saving substantial testing. As stated before, a secondary structure interpretation of UAS could be very powerful in reducing certification burden. Sophisticated analytical techniques that require exceptionally skilled personnel and software modeling that cost thousands a month are still less expensive than testing airframes that cost thousands of dollars an hour to operate. Some envelope and stability testing will still be required, but a majority of rules could be shown compliant on paper without the need for physical verification. Proof of Compliance, Proof of Structure, and Proof of

Strength rules should be modified for a total secondary structure aircraft that would allow a higher amount of proof to be generated analytically.

6. Summary and Conclusion

The Air Force data acquired provides a broad picture of the current state of UAS reliability. The AFSC data is complete in its number, but obscure in its detail. The AIB executive summaries lack completeness, but provide a much stronger narrative into the causes of individual events. The comparison of the data showed conflict that can only be resolved with more complete data, but it shows the accuracy of each set. The figures contained in this thesis show that reliability is improving, but at a rate that is unacceptable for FAA certification in the next few decades. Non-catastrophic mishap rate are shown to be flat, indicating some systemic change need to happen to address these lesser modes of failure before improvement will be seen. The MQ-1/ RQ-1 while causing the greatest number of incidents has also achieved the most fleet experience. Its reliability is not an extreme outlier to the other vehicles in this study vehicles. Some maturity of design is showing newer platforms fielded, but the spread in mishap rates is still tightly banded.

Physical reliability stood out as the largest cause on mishap across the fleet. The cause of many of the Class A losses is Powerplant failures. Further look in these failures showed broad sources that will not be addressed simply. Other manned causes of failure include lack of determinate assembly of components and lack of residual control of aircraft. The failures found show a lack of compliance to existing 14CFR rules and show enforcement of existing rules will be largely sufficient to improve reliability. Still, new airworthiness issues are revealed in the study. The environmental sensitivity of the vehicles is higher than manned aircraft due to high surface to mass ratios. Also, the remoteness of command and perception must be address through new regulations and new technology.

Compliance to the rules set forth is shown possible through traditional means. Pure flight testing of these UAS to compliance is possible and divulges little information to public records, but it will come at a high resource cost. Because of the reduced risk these platforms pose when confidently controlled, a modification of existing proof rules is suggested to consider the entire airframe Secondary structure. This will severely reduce the cost of Type certification of future UAS and will make existing applicable Part 25 Rules very suitable as a basis for UAS rulemaking.

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AGRICULTURAL AIPLANES", AC21.25-1. U.S. Department of Transportation, Federal Aviation Administration, 1 December 1997.
PART 25—AIRWOR TRANSPORT CATE(RTH GOR	INE Y A	CSS S IRP	STA LAN	NDA ES	ARD	S:											
	Le Dulo	Applicable to		DA Floot	History	Applicability		Flight Test			Ground Test / Inspection	4		Drawings	Keview	Work Needed	Coverage	erage
	Complete	No	Partial	Complete	No	Partial	Complete	No	Partial	Complete	No	Partial	Complete	No	Partial	Additional	Complete C	Partial Cov
Subpart A—																		
General	*		*															
	*		*															
§ 25.1 Applicability.	1				1			1				1			1			1
§ 25.2 Special retroactive			1															
§ 25.3 Special provisions			1															
for ETOPS type design																		
approvals.			1															
§ 25.5 Incorporations by	1				1			1				1			1			1
	*		*		1			1				1			1			1
Subnart B—Flight	*		*															
Suspirio ingli	*		*															

Appendix A: 14CFR Part25 Applicability and Sufficiency of Means of Compliance

	Ic Dula	Applicable to		DA Floot	History	Applicability		Flight Test			Ground Test / Inspection	4	/ - : - - • •	Aniaysis/ Drawings	Kevlew	Work Needed	Coverage	erage
	Complete	No	Partial	Complete	No	Partial	Complete	No	Partial	Complete	No	Partial	Complete	No	Partial	Additional	Complete (Partial Cov
General	*		*															
§ 25.21 Proof of																		
compliance.	1					1			1			1			1			1
§ 25.23 Load distribution					1						1				1		4	
limits. 8 25 25 Weight limits	1				1 1		1				1				1 1		1 1	
§ 25.25 Weight limits.	1				1		1				1				1		1	
§ 25.27 Center of gravity	1				1		1				1				1		1	
§ 25.29 Empty weight and corresponding center of	1				1		1				1				1		Ĩ	
gravity.	1				1			1		1					1		1	
§ 25.31 Removable ballast.§ 25.33 Propeller speed	1				1		1			1					1		1	
and pitch limits.	1				1		1			1					1		1	
	*		*															
Performance	*		*															
§ 25.101 General.	1				1			1				1			1			1
§ 25.103 Stall speed.	1				1		1				1				1		1	
§ 25.105 Takeoff.	1				1		1				1				1		1	
§ 25.107 Takeoff speeds.	1				1		1				1				1		1	
§ 25.109 Accelerate-stop																		
distance.	1				1		1				1				1		1	

	Ic Dula	Applicable to		DA Float	History	Applicability		Flight Test			Ground Test / Inspection			Aniaysis/ Drawings	Kevlew	Work Needed	Coverage	erage
	Complete	No	Partial	Complete	No	Partial	Complete	No	Partial	Complete	No	Partial	Complete	No	Partial	Additional	Complete (Partial Cov
§ 25.111 Takeoff path.	1				1		1				1				1		1	
§ 25.113 Takeoff distance																		
and takeoff run.	1				1		1				1				1		1	
§ 25.115 Takeoff flight	1				1		1				1				1		1	
path. 8 25 117 Climb: general					1		1				1				1		1	
\$ 25.117 Clinib. general.	1				1		1				1				1		1	
All-engines-operating.	1				1		1				1				1		1	
§ 25.121 Climb: One-											_				_			
engine-inoperative.	1				1		1				1				1		1	
§ 25.123 En route flight																		
paths.	1				1		1				1				1		1	
§ 25.125 Landing.	1				1		1				1				1		1	
	*		*															
Controllability and																		
Maneuverability	*		*															
§ 25.143 General.	1				1		1				1				1		1	
§ 25.145 Longitudinal	1				1		1				1				1		1	
8 25 147 Directional and	1				1		1				1				1		1	
lateral control.	1				1		1				1				1		1	

	Is Rule	Applicable to		DA Fleet	History	Аррисаонну		Flight Test			Ground Test / Inspection		A 11 000010/	Drawings	Kevlew	Work Needed	Coverage	erage
	Complete	No	Partial	Complete	No	Partial	Complete	No	Partial	Complete	No	Partial	Complete	No	Partial	Additional	Complete (Partial Cov
§ 25.149 Minimum control																		
speed.	1				1		1				1				1		1	
	*		*															
Trim	*		*															
§ 25.161 Trim.	1				1		1					1			1		1	
	*		*															
Stability	*		*															
§ 25.171 General.	1				I			I			I				I	1		
§ 25.173 Static	1				1		1				1				1		1	
Solution and stability.	1				1		1				1				1		1	
§ 25.1/5 Demonstration of static longitudinal stability	1				1		1				1				1		1	
8 25 177 Static lateral	1				1		1				1				1		1	
directional stability	1				1		1				1				1		1	
§ 25.181 Dynamic	-						•				•						•	
stability.	1				1		1				1				1		1	
	*		*															
Stalls	*		*															
§ 25.201 Stall																		
demonstration.	1				1		1				1				1		1	
§ 25.203 Stall	1				1		1				1				1		1	
characteristics.	1				1		1				1				1		1	

	Le Dula	Applicable to		DA Float	History	Applicability		Flight Test			Ground Test / Inspection		A aloroio/	Drawings	Kevlew	Work Needed	Coverage	erage
	Complete	No	Partial	Complete	No	Partial	Complete	No	Partial	Complete	No	Partial	Complete	No	Partial	Additional	Complete (Partial Cov
§ 25.207 Stall warning.	1 *		*		1		1					1		1			1	
Ground and Water Handling Characteristics § 25.231 Longitudinal	*		*															
stability and control. § 25.233 Directional	1				1		1				1				1		1	
stability and control. § 25.235 Taxiing	1				1		1			1					1		1	
condition. § 25.237 Wind velocities.	1 1				1 1		1 1				1 1				1 1		1 1	
§ 25.239 Spray characteristics, control, and stability on water.	*		1 *		1		-				-				-		-	
Miscellaneous Flight																		
Requirements	*		*															
buffeting.	1				1		1				1				1		1	
§ 25.253 High-speed characteristics.	1				1		1				1				1		1	

	L, Dulo	Applicable to		DA Floot	History	Applicability		Flight Test			Ground Test / Inspection		A aloroio/	Drawings	Kevlew	Work Needed	Coverage	erage
	Complete	No	Partial	Complete	No	Partial	Complete	No	Partial	Complete	No	Partial	Complete	No	Partial	Additional	Complete (Partial Cov
§ 25.255 Out-of-trim																		
characteristics.	1 *		*		1		1				1				1		1	
Subpart C—																		
Structure	*		*															
	*		*															
	*		*															
General	*		*															
§ 25.301 Loads	1				1		1				1				1		1	
§ 25.303 Factor of safety.	1				1		1			1	-				1		1	
8 25 305 Strength and	-				-		-			-					-		-	
deformation.	1				1		1				1		1				1	
§ 25.307 Proof of																		
structure.	1				1		1			1			1				1	
	*		*															
Flight Loads	*		*															
§ 25.321 General.	1				1		1				1				1		1	
	*		*															
Flight Maneuver and																		
Gust Conditions	*		*															

	Ic Dula	Applicable to	UAV (DA Floot	History	Applicability		Flight Test			Ground Test / Inspection		\	Drawings	Kevlew	Work Needed	loverage	erage
	Complete	No	Partial	Complete	No	Partial	Complete	No	Partial	Complete	No	Partial	Complete	No	Partial	Additional	Complete (Partial Cov
§ 25.331 Symmetric																		
maneuvering conditions.	1				1		1				1				1		1	
§ 25.333 Flight																		
maneuvering envelope.	1				1		1				1		1				1	
§ 25.335 Design airspeeds.	1				1		1				1		1				1	
§ 25.337 Limit																		
maneuvering load factors.	1				1		1				1				1		1	
§ 25.341 Gust and																		
turbulence loads.	1					1	1				1				1		1	
§ 25.343 Design fuel and	1				1			1			1				1	1		
011 loads.	1		1		I			I			1				I	1		
§ 25.345 High lift devices.			I															
conditions	1				1		1				1				1		1	
8 25 351 Vaw maneuver	1				1		1				1				1		1	
conditions	1				1		1				1				1		1	
	*		*		-		-				-				-		-	
Supplementary																		
Conditions	*		*															
§ 25.361 Engine torque.	1				1			1		1					1		1	

	Ic Dulo	Applicable to		DA Floot	History	Applicability		Flight Test			Ground Test / Inspection		/ -: V	Anaysis/ Drawings	Keview	Work Needed	loverage	erage
	Complete	No	Partial	Complete	No	Partial	Complete	No	Partial	Complete	No	Partial	Complete	No	Partial	Additional	Complete (Partial Cov
§ 25.363 Side load on engine and auxiliary power																		
unit mounts.	1				1		1			1					1		1	
§ 25.365 Pressurized compartment loads.			1															
§ 25.367 Unsymmetrical																		
loads due to engine failure.	1				1		1				1				1		1	
§ 25.371 Gyroscopic loads.	1				1		1				1				1		1	
§ 25.373 Speed control																		
devices.			1															
	*		*															
Control Surface and																		
System Loads	*		*															
§ 25.391 Control surface	1				1		1				1				1		1	
loads: General.	1				1		1				1				I		1	
§ 25.393 Loads parallel to	1				1		1				1				1		1	
8 25 395 Control system	1				1		1				1				1		1	
\$ 25.393 Control system	1				1		1				1				1		1	
loads.	1				1		1				1				1		1	

	Le Dula	Applicable to	UAV?	DA Floot	History	Аррисаонну		Flight Test			Ground Test / Inspection		\	Drawings	Kevlew	Work Needed	Coverage	erage
	Complete	No	Partial	Complete	No	Partial	Complete	No	Partial	Complete	No	Partial	Complete	No	Partial	Additional	Complete (Partial Cov
§ 25.399 Dual control																		
system.			1															
§ 25.405 Secondary																		
control system.			1															
§ 25.407 Trim tab effects.	1				1		1				1				1		1	
§ 25.409 Tabs.	1				1		1			1					1		1	
§ 25.415 Ground gust	1				1		1				1				1		1	
conditions.	1				1		1				1				I		I	
§ 25.427 Unsymmetrical	1				1		1				1				1		1	
10aus.	1				1		1				1				1		1	
aerodynamic surfaces			1															
§ 25.457 Wing flaps.			1															
§ 25.459 Special devices.	1		_		1			1			1				1	1		
° 1	*		*															
Ground Loads	*		*															
§ 25.471 General.	1				1			1			1				1	1		
§ 25.473 Landing load																		
conditions and assumptions.	1				1		1				1				1		1	
§ 25.477 Landing gear																		
arrangement.	1				1		1				1				1		1	

	Ic Rule	Applicable to		DA Fleet	History	Applicability		Flight Test			Ground Test / Inspection		An1 000010/	Drawings	Kevlew	Work Needed	Coverage	erage
	Complete	No	Partial	Complete	No	Partial	Complete	No	Partial	Complete	No	Partial	Complete	No	Partial	Additional	Complete (Partial Cov
§ 25.479 Level landing																		
conditions.	1				1		1				1				1		1	
§ 25.481 Tail-down																		
landing conditions.	1				1		1				1				1		1	
§ 25.483 One-gear landing																		
conditions.	1				1		1				1				1		1	
§ 25.485 Side load	1				1		1				1				1		1	
conditions.	1				1		1				1				1		1	
§ 25.487 Rebound landing	1				1		1				1				1		1	
8 25 480 Crownd handling	1				1		1				1				1		1	
§ 23.489 Ground handling	1				1			1		1					1		1	
8 25 401 Taxi takeoff and	1				1			1		1					1		1	
anding roll.	1				1		1				1				1		1	
8 25 493 Braked roll	-				-		-				-				-		-	
conditions.	1				1		1				1				1		1	
§ 25.495 Turning.	1				1			1		1					1		1	
§ 25.497 Tail-wheel																		
yawing.	1				1			1		1					1		1	
§ 25.499 Nose-wheel yaw																		
and steering.	1				1			1		1					1		1	
§ 25.503 Pivoting.	1				1			1		1					1		1	

	Le Dulo	Applicable to	2 A W O	DA Floot	History	Applicability		Flight Test			Ground Test / Inspection		A aloroio/	Drawings	Review	Work Needed	Coverage	erage
	Complete	No	Partial	Complete	No	Partial	Complete	No	Partial	Complete	No	Partial	Complete	No	Partial	Additional	Complete (Partial Cov
§ 25.507 Reversed																		
braking.	1				1			1		1					1		1	
§ 25.509 Towing loads.	1				1			1		1					1		1	
§ 25.511 Ground load: unsymmetrical loads on multiple-wheel units.	1				1		1			1					1		1	
§ 25.519 Jacking and tie-																		
down provisions.	1				1			1		1					1		1	
	*		*															
Water Loads	*		*															
§ 25.521 General.			1															
§ 25.523 Design weights																		
and center of gravity			1															
8 25 525 Application of			1															
loads.			1															
§ 25.527 Hull and main																		
float load factors.			1															
§ 25.529 Hull and main																		
float landing conditions.			1															
§ 25.531 Hull and main																		
float takeoff condition.			1															

	Ic Rule	Applicable to		DA Floot	History	Applicaulity		Flight Test			Ground Test / Inspection		Anloweis/	Drawings	Kevlew	Work Needed	Coverage	erage
	Complete	No	Partial	Complete	No	Partial	Complete	No	Partial	Complete	No	Partial	Complete	No	Partial	Additional	Complete (Partial Cov
 § 25.533 Hull and main float bottom pressures. § 25.535 Auxiliary float loads. § 25.537 Seawing loads. 	*		1 1 1 *															
Emergency Landing Conditions	*		*															
§ 25.561 General.§ 25.562 Emergency landing dynamic conditions.			1															
§ 25.563 Structural ditching provisions.	*		1															
Fatigue Evaluation	*		*															
§ 25.571 Damage— tolerance and fatigue evaluation of structure.	1		ł			1	1			1					1		1	
Lightning Protection § 25.581 Lightning	*		*															
protection.	1					1	1					1			1		1	

	Ic Rule	Applicable to	: 100	DA Floot	History	Applicability		Flight Test			Ground Test / Inspection		A aloroio/	Drawings	Kevlew	Work Needed	Coverage	erage
	Complete	No	Partial	Complete	No	Partial	Complete	No	Partial	Complete	No	Partial	Complete	No	Partial	Additional	Complete (Partial Cov
Subpart D—Design																		
and Construction	*		*															
	*		*															
	*		*															
General	*		*															
§ 25.601 General.	1				1			1				1			1			1
§ 25.603 Materials.	1				1			1		1					1		1	
§ 25.605 Fabrication															_			
methods.	1				1			1		1					1		1	
§ 25.607 Fasteners.	1				1			1		1					1		1	
§ 25.609 Protection of	1				1			1		1					1		1	
8 25 611 Accessibility	1				1			1		1					1		1	
provisions.	1				1			1		1			1				1	
§ 25.613 Material strength	-				-			-		-			-				-	
design values	1				1			1		1			1				1	
§ 25.619 Special factors.	1				1			1			1		1			1	-	
§ 25.621 Casting factors.	1				1			1		1	-		1				1	
§ 25.623 Bearing factors.	1				1			1		1			1				1	
§ 25.625 Fitting factors.	1				1			1		1			1				1	

	Ic Dula	Applicable to		DA Fleet	History	Аррисаниу		Flight Test			Ground Test / Inspection		Antorrio/	Drawings	Kevlew	Work Needed	Coverage	erage
	Complete	No	Partial	Complete	No	Partial	Complete	No	Partial	Complete	No	Partial	Complete	No	Partial	Additional	Complete (Partial Cov
§ 25.629 Aeroelastic																		
stability requirements.	1				1		1				1				1		1	
g 25.051 Bird strike damage.	1					1		1		1			1			1		
	*		*							_			_					
Control Surfaces	*		*															
§ 25.651 Proof of strength.	1				1		1			1					1		1	
§ 25.655 Installation.	1				1			1		1					1		1	
§ 25.657 Hinges.	1				1			1		1					1		1	
~	*		*															
Control Systems	*		*															
§ 25.671 General.	1				1			1			1				1	1		
§ 25.072 Stability																		
and power-operated																		
systems.	1				1		1					1			1		1	
§ 25.675 Stops.	1				1		1			1					1		1	
§ 25.677 Trim systems.	1				1		1				1				1		1	
§ 25.679 Control system																		
gust locks.	1				1		1			1					1		1	
§ 25.681 Limit load static																		
tests.	1				1		1			1					1		1	

	Ic Rula	Applicable to		DA Float	History	Аррисаонцу		Flight Test			Ground Test / Inspection			Drawings D	Kevlew	Work Needed	Coverage	erage
	Complete	No	Partial	Complete	No	Partial	Complete	No	Partial	Complete	No	Partial	Complete	No	Partial	Additional	Complete (Partial Cov
§ 25.683 Operation tests.	1				1		1					1			1		1	
§ 25.685 Control system																		
details.	1				1		1					1			1		1	
§ 25.689 Cable systems.	1				1				1	1					1		1	
§ 25.693 Joints.	1				1			1		1					1		1	
§ 25.697 Lift and drag																		
devices, controls.			1															
§ 25.699 Lift and drag																		
device indicator.			1															
§ 25.701 Flap and slat			1															
interconnection.			1															
§ 25.703 Takeoff warning	1				1		1				1				1		1	
system.	1 *		*		1		1				1				1		1	
Landing Gear	*		*															
8 25 721 General	1		•		1			1			1				1	1		
§ 25.721 General.	1				1			1			1				1	1		
§ 25.725 Shock absorption	1				1		1			1					1		1	
8 25 729 Retracting	1				1		T			T					1		T	
mechanism.	1				1				1	1					1		1	
§ 25.731 Wheels.	1				1				1	1					1		1	

	I, D.J.	Applicable to		DA Float	History	Applicability		Flight Test			Ground Test / Inspection		/ -: V	Drawings	Kevlew	Work Needed	Coverage	erage
	Complete	No	Partial	Complete	No	Partial	Complete	No	Partial	Complete	No	Partial	Complete	No	Partial	Additional	Complete (Partial Cov
§ 25.733 Tires.	1				1				1	1					1		1	
§ 25.735 Brakes and																		
braking systems.	1				1				1	1					1		1	
§ 25.737 Skis.			1															
	*		*															
Floats and Hulls	*		*															
§ 25.751 Main float																		
buoyancy.			1															
§ 25./53 Main float			1															
8 25 755 Hulls			1															
§ 25.755 Thuns.	*		1 *															
Personnal and Canac																		
Accommodations	*		*															
8 25 771 Pilot			-															
compartment.			1															
§ 25.772 Pilot																		
compartment doors.			1															
§ 25.773 Pilot																		
compartment view.			1															

	Is Rule	Applicable to		DA Floot	History	Applicability		Flight Test			Ground Test / Inspection		Anlaweie/	Drawings	Review	Work Needed	Coverage	erage
	Complete	No	Partial	Complete	No	Partial	Complete	No	Partial	Complete	No	Partial	Complete	No	Partial	Additional	Complete (Partial Cov
§ 25.775 Windshields and																		
windows.			1															
§ 25.777 Cockpit controls.			1															
§ 25.779 Motion and effect																		
of cockpit controls.			1															
§ 25.781 Cockpit control																		
knob shape.			1															
§ 25.783 Fuselage doors.			1															
§ 25.785 Seats, berths,																		
safety belts, and harnesses.			1															
§ 25.787 Stowage																		
compartments.			1															
§ 25.789 Retention of																		
items of mass in passenger																		
and crew compartments and			1															
galleys. 8 25 701 Passenger			1															
information signs and																		
placards.			1															
§ 25.793 Floor surfaces.			1															
§ 25.795 Security																		
considerations.			1															

	1, D.1,	Applicable to			History	Applicability		Flight Test			Ground Test / Inspection	ı	A aloroio/	Drawings	Kevlew	Work Needed	Coverage	erage
	Complete	No	Partial	Complete	No	Partial	Complete	No	Partial	Complete	No	Partial	Complete	No	Partial	Additional	Complete (Partial Cov
	*		*															
Emergency Provisions	*		*															
§ 25.801 Ditching.			1															
§ 25.803 Emergency																		
evacuation.			1															
§ 25.807 Emergency exits.			1															
§ 25.809 Emergency exit																		
arrangement.			1															
§ 25.810 Emergency																		
egress assist means and																		
escape routes.			1															
§ 25.811 Emergency exit			1															
marking.			1															
§ 25.812 Emergency			1															
8 25 813 Emorgonov ovit			1															
access			1															
8 25.815 Width of aisle			1															
8 25 817 Maximum			1															
number of seats abreast.			1															

	La Dulo	Applicable to	UAV :	DA Floot	History	Applicability		Flight Test			Ground Test / Inspection		Anlausi s/	Drawings	Kevlew	Work Needed	Coverage	erage
	Complete	No	Partial	Complete	No	Partial	Complete	No	Partial	Complete	No	Partial	Complete	No	Partial	Additional	Complete (Partial Cov
§ 25.819 Lower deck service compartments (including galleys).§ 25.820 Lavatory doors.	*		1 1 *															
Ventilation and Heating § 25.831 Ventilation. § 25.832 Cabin ozone concentration. § 25.833 Combustion heating systems.	*		* 1 1															
Pressurization § 25.841 Pressurized cabins. § 25.843 Tests for pressurized cabins.	* *		* 1 1 *															
<i>Fire Protection</i> § 25.851 Fire extinguishers.	*		*															

	La Dulo	Applicable to	UAV :	DA Floot	History	Applicability		Flight Test			Ground Test / Inspection		A 11 00010 /	Drawings	Kevlew	Work Needed	Coverage	erage
	Complete	No	Partial	Complete	No	Partial	Complete	No	Partial	Complete	No	Partial	Complete	No	Partial	Additional	Complete (Partial Cov
§ 25.853 Compartment			1															
§ 25.854 Lavatory fire protection.			1															
§ 25.855 Cargo or baggage compartments.			1															
§ 25.856 Thermal/Acoustic insulation materials.			1															
§ 25.857 Cargo compartment classification.			1															
§ 25.858 Cargo or baggage compartment smoke or fire																		
detection systems.			1															
heater fire protection.			1															
§ 25.865 Fianinable fluid fire protection.			1															
§ 25.865 Fire protection of flight controls, engine																		
mounts, and other flight structure.			1															

	Lo Dulo	Applicable to		DA Floot	History	Applicability		Flight Test			Ground Test / Inspection		Anl ansia/	Drawings Drawings	NEVIEW	Work Needed	Coverage	erage
	Complete	No	Partial	Complete	No	Partial	Complete	No	Partial	Complete	No	Partial	Complete	No	Partial	Additional	Complete C	Partial Cov
§ 25.867 Fire protection:																		
other components.			1															
§ 25.869 Fire protection:			1															
systems.	*		1 *															
Miscellaneous	*		*															
8 25 871 Leveling means	1		•		1		1					1			1		1	
8 25 875 Reinforcement	1				1		1					1			1		1	
near propellers.	1				1				1	1					1		1	
§ 25.899 Electrical																		
bonding and protection																		
against static electricity.	1				1			1		1					1		1	
	*		*															
Subpart E—																		
Powerplant	*		*															
I I I I I	*		*															
	*		*															
General	*		*															
§ 25.901 Installation.	1				1			1		1					1		1	
§ 25.903 Engines.	1				1			1		1					1		1	

	Le Dula	Applicable to		DA Floot	History	Аррисаниу		Flight Test			Ground Test / Inspection			Drawings	Kevlew	Work Needed	Coverage	erage
	Complete	No	Partial	Complete	No	Partial	Complete	No	Partial	Complete	No	Partial	Complete	No	Partial	Additional	Complete (Partial Cov
§ 25.904 Automatic																		
takeoff thrust control system	1				1		1				1				1		1	
(ATTCS). 8 25 005 Propellars	1				1 1		1			1	1				1 1		1	
§ 25.905 Propeller	1				1		1			1					1		1	
vibration and fatigue	1				1		1			1					1		1	
§ 25.925 Propeller	-				•		•			-					•		1	
clearance.	1				1		1			1					1		1	
§ 25.929 Propeller deicing.			1															
§ 25.933 Reversing	4				1				1						1			0
systems.	1				I				I			1			1		I	0
§ 25.934 Turbojet engine	1				1				1			1			1		1	0
8 25 937 Turbopropeller	1				1				1			1			1		1	0
drag limiting systems.			1															
§ 25.939 Turbine engine			-															
operating characteristics.	1				1		1			1					1		1	
§ 25.941 Inlet, engine, and																		
exhaust compatibility.	1				1			1		1					1		1	
§ 25.943 Negative																		
acceleration.	1				1		1				1				1		1	

	Le Dula	Applicable to		DA Floot	History	Applicaulity		Flight Test			Ground Test / Inspection			Drawings	Kevlew	Work Needed	Coverage	erage
	Complete	No	Partial	Complete	No	Partial	Complete	No	Partial	Complete	No	Partial	Complete	No	Partial	Additional	Complete (Partial Cov
§ 25.945 Thrust or power																		
augmentation system.	1				1		1					1			1		1	
	*		*															
Fuel System	*		*															
§ 25.951 General.	1				1			1			1				1	1		
§ 25.952 Fuel system																		
analysis and test.	1				1		1			1					1		1	
§ 25.953 Fuel system																		
independence.	1				1		1			1					1		1	
§ 25.954 Fuel system																		
lightning protection.	1				1			1		1					1		1	
§ 25.955 Fuel flow.	1				1		1					1			1		1	
§ 25.957 Flow between	1				1		1					1			1		1	
interconnected tanks.	1				1		1					1			1		1	
§ 25.959 Unusable fuel	1				1		1			1					1		1	
supply.	1				1		1			1					1		1	
§ 25.961 Fuel system not	1				1		1			1					1		1	
8 25 963 Fuel tanks	1				1		1			1					1		1	
general.	1				1			1			1				1	1		
§ 25.965 Fuel tank tests.	1				1			1		1					1		1	

	Ic Bula	Applicable to		DA Fleet	History	Аррисаонну		Flight Test			Ground Test / Inspection		A 51 0.000	Drawings	Kevlew	Work Needed	Coverage	erage
	Complete	No	Partial	Complete	No	Partial	Complete	No	Partial	Complete	No	Partial	Complete	No	Partial	Additional	Complete (Partial Cov
§ 25.967 Fuel tank																		
installations.	1				1			1		1					1		1	
§ 25.969 Fuel tank																		
expansion space.	1				1			1		1					1		1	
§ 25.971 Fuel tank sump.	1				1			1		1					1		1	
§ 25.973 Fuel tank filler																		
connection.	1				1			1		1					1		1	
§ 25.975 Fuel tank vents																		
and carburetor vapor vents.	1				1			1		1					1		1	
§ 25.977 Fuel tank outlet.	1				1			1		1					1		1	
§ 25.979 Pressure fueling																		
system.	1				1		1			1					1		1	
§ 25.981 Fuel tank ignition																		
prevention.	1				1			1		1					1		1	
	*		*															
Fuel System Components	*		*															
§ 25.991 Fuel pumps.	1				1			1		1					1		1	
§ 25.993 Fuel system lines																		
and fittings.	1				1		1			1					1		1	
§ 25.994 Fuel system																		
components.	1				1			1		1					1		1	

	Ic Dula	Applicable to		DA Fleet	History	Applicability		Flight Test			Ground Test / Inspection			Aniaysis/ Drawings	Keview	Work Needed	Coverage	erage
	Complete	No	Partial	Complete	No	Partial	Complete	No	Partial	Complete	No	Partial	Complete	No	Partial	Additional	Complete (Partial Cov
§ 25.995 Fuel valves.	1				1		1			1					1		1	
§ 25.997 Fuel strainer or																		
filter.	1				1		1			1					1		1	
§ 25.999 Fuel system drains.	1				1		1			1					1		1	
§ 25.1001 Fuel jettisoning																		
system.	1				1		1			1					1		1	
	*		*															
Oil System	*		*															
§ 25.1011 General.	1				1			1			1				1	1		
§ 25.1013 Oil tanks.	1				1			1		1					1		1	
§ 25.1015 Oil tank tests.	1				1			1		1					1		1	
§ 25.1017 Oil lines and																		
fittings.	1				1			1		1					1		1	
§ 25.1019 Oil strainer or																		
filter.	1				1			1		1					1		1	
g 25.1021 On system	1				1			1		1					1		1	
8 25 1023 Oil radiators	1				1		1	1		1					1		1	
§ 25.1025 Oil valves	1				1		1	1		1					1		1	
§ 25.1027 Propeller	-				-			-		-					-		-	
feathering system.	1				1		1			1					1		1	

	I _c Dulo	Applicable to		DA Eloot	History	Applicability		Flight Test			Ground Test / Inspection	1	/ -	Anlaysis/ Drawings	Kevlew	Work Needed	Coverage	erage
	Complete	No	Partial	Complete	No	Partial	Complete	No	Partial	Complete	No	Partial	Complete	No	Partial	Additional	Complete (Partial Cov
	*		*															
Cooling	*		*															
§ 25.1041 General.	1				1			1			1				1	1		
§ 25.1043 Cooling tests.	1				1		1			1					1		1	
§ 25.1045 Cooling test																		
procedures.	1				1		1			1					1		1	
	*		*															
Induction System	*		*		1		1			1					1		1	
§ 25.1091 Air induction.	1				I		1			1					1		1	
§ 25.1093 Induction			1		1		1			1					1			
8 25 1101 Carburator air			1		1		1			1					1			
g 23.1101 Carburetor all	1				1		1				1				1		1	
§ 25.1103 Induction					1		1				1				1		1	
system ducts and air duct																		
systems.	1				1		1			1					1		1	
§ 25.1105 Induction																		
system screens.	1				1				1	1					1		1	
§ 25.1107 Inter-coolers					_													
and after-coolers.	1				1		1				1				1		1	
	*		*	I									I					

	Le Dula	Applicable to	UAV?	DA Floot	History	Аррисаонну		Flight Test			Ground Test / Inspection		A 1 100010 /	Drawings Drawings	Kevlew	Work Needed	Coverage	erage
	Complete	No	Partial	Complete	No	Partial	Complete	No	Partial	Complete	No	Partial	Complete	No	Partial	Additional	Complete (Partial Cov
Exhaust System	*		*															
§ 25.1121 General.	1				1			1			1				1	1		
§ 25.1123 Exhaust piping.	1				1				1	1					1		1	
§ 25.1125 Exhaust heat																		
exchangers.	1				1				1	1					1		1	
§ 25.1127 Exhaust driven																		
turbo-superchargers.	1				1				1	1					1		1	
	*		*															
Powerplant Controls and																		
Accessories	*		*															
§ 25.1141 Powerplant	1				1		1					1			1		1	
controls: general.	1				1		1					I			1		I	
§ 25.1142 Auxiliary power	1				1		1			1					1		1	
8 25 1143 Engine controls	1				1		1			1		1			1		1	
§ 25.1145 Englie Controls. 8 25.1145 Ignition	1				1		1					1			1		1	
switches.	1				1		1					1			1		1	
§ 25.1147 Mixture																		
controls.	1				1		1			1					1		1	
§ 25.1149 Propeller speed																		
and pitch controls.	1				1		1					1			1		1	

	L, Dulo	Applicable to		DA Floot	History	Applicability		Flight Test			Ground Test / Inspection		Anlaweic/	Drawings	Kevlew	Work Needed	loverage	erage
	Complete	No	Partial	Complete	No	Partial	Complete	No	Partial	Complete	No	Partial	Complete	No	Partial	Additional	Complete C	Partial Cov
§ 25.1153 Propeller feathering controls.	1				1		1					1			1		1	
 § 25.1155 Reverse thrust and propeller pitch settings below the flight regime. § 25.1157 Carburetor air 	1				1		1			1		-			1		1	
temperature controls.			1															
controls.	1				1		1					1			1		1	
§ 25.1161 Fuel jettisoning system controls.§ 25.1163 Powerplant	1				1		1					1			1		1	
accessories.	1				1		1					1			1		1	
systems.	1				1		1					1			1		1	
g 25.1167 Accessory gearboxes.	1 *		*		1		1			1					1		1	

	Ic Dula	Applicable to	; A 1 0	DA Fleet	History	Applicability		Flight Test			Ground Test / Inspection		A sloveio/	Drawings	Kevlew	Work Needed	Coverage	erage
	Complete	No	Partial	Complete	No	Partial	Complete	No	Partial	Complete	No	Partial	Complete	No	Partial	Additional	Complete (Partial Cov
Powerplant Fire																		
Protection	*		*															
§ 25.1181 Designated fire zones; regions included.	1				1			1		1					1		1	
§ 25.1182 Nacelle areas behind firewalls, and engine pod attaching structures containing flammable fluid																		
lines.			1															
§ 25.1183 Flammable																		
fluid-carrying components. § 25.1185 Flammable	1				1			1		1					1		1	
fluids.	1				1			1		1					1		1	
§ 25.1187 Drainage and																		
ventilation of fire zones.	1				1			1		1					1		1	
§ 25.1189 Shutoff means.	1				1		1			1					1		1	
§ 25.1191 Firewalls.	1				1			1		1					1		1	
§ 25.1192 Engine																		
accessory section			1															
diaphragm.			1															
§ 25.1195 Cowling and	1				1		1			1					1		1	
nacelle skin.	1				1		1			1					1		1	

	Lo Dulo	Applicable to	UAV (DA Floot	History	Applicability		Flight Test			Ground Test / Inspection		/ -: V	Aniaysis/ Drawings	Kevlew	Work Needed	loverage	erage
	Complete	No	Partial	Complete	No	Partial	Complete	No	Partial	Complete	No	Partial	Complete	No	Partial	Additional	Complete (Partial Cov
§ 25.1195 Fire			1															
8 25 1197 Fire			1															
extinguishing agents.			1															
§ 25.1199 Extinguishing																		
agent containers.			1															
§ 25.1201 Fire																		
materials.			1															
§ 25.1203 Fire detector																		
system.	1				1		1			1					1		1	
§ 25.1207 Compliance.			1															
	*		*															
Subpart F—																		
Equipment	*		*															
	*		*															
~ .	*		*															
General	*		*															
§ 25.1301 Function and	1				1		1			1					1		1	
installation.	1				1		1			1					1		1	

	Le Dula	Applicable to		DA Floot	History	Applicability		Flight Test			Ground Test / Inspection			Drawings	Kevlew	Work Needed	Coverage	erage
	Complete	No	Partial	Complete	No	Partial	Complete	No	Partial	Complete	No	Partial	Complete	No	Partial	Additional	Complete (Partial Cov
§ 25.1303 Flight and																		
navigation instruments.	1				1		1				1				1		1	
§ 25.1305 Powerplant	1				1		1				1				1		1	
8 25 1207 Missellaneous	1				1		1				1				1		1	
equipment.	1				1		1				1				1		1	
§ 25.1309 Equipment,																		
systems, and installations.	1				1		1			1					1		1	
§ 25.1310 Power source																		
capacity and distribution.	1				1			1		1					1		1	
§ 25.1316 System	1				1				1	1					1		1	
S 25 1217 High intensity	1				1				1	1					1		1	
8 25.1517 Hign-Intensity Radiated Fields (HIRF)																		
Protection.	1				1		1			1					1		1	
	*		*															
Instruments: Installation	*		*															
§ 25.1321 Arrangement																		
and visibility.			1															
§ 25.1322 Flightcrew			_															
alerting.			1															

	Lo Dulo	Applicable to		DA Floot	History	Applicability		Flight Test			Ground Test / Inspection			Drawings Drawings	Kevlew	Work Needed	Coverage	erage
	Complete	No	Partial	Complete	No	Partial	Complete	No	Partial	Complete	No	Partial	Complete	No	Partial	Additional	Complete (Partial Cov
§ 25.1323 Airspeed																		
indicating system.	1				1			1		1					1		1	
§ 25.1325 Static pressure																		
systems.	1				1			1		1					1		1	
§ 25.1326 Pitot heat																		
indication systems.	1				1		1			1				1			1	
§ 25.1327 Magnetic																		
direction indicator.			1															
§ 25.1329 Flight guidance	1				1			1		1					1		4	
system.	1				I			I		1					1		I	
§ 25.1331 Instruments	1				1		1			1					1		1	
using a power supply.	1				1		1			1					1		1	
§ 25.1333 Instrument	1				1		1			1					1		1	
8 25 1327 Dowornlant	1				1		1			1					1		1	
§ 25.1557 Fowerplant	1				1		1			1					1		1	
instruments.	*		*		1		1			1					1		1	
Flastriad Systems and																		
Enectrical Systems and Fauinment	*		*															
§ 25.1351 General.	1				1			1			1				1	1		

	L _c Dulo	Applicable to		DA Floot	History	Applicability		Flight Test			Ground Test / Inspection		/-:	Aniaysis/ Drawings	Kevlew	Work Needed	loverage	erage
	Complete	No	Partial	Complete	No	Partial	Complete	No	Partial	Complete	No	Partial	Complete	No	Partial	Additional	Complete C	Partial Cov
§ 25.1353 Electrical																		
equipment and installations.	1				1			1		1					1		1	
§ 25.1355 Distribution																		
system.	1				1			1		1					1		1	
§ 25.1357 Circuit	1				1			1		1					1		1	
protective devices.	1				1			1		1					1		1	
§ 25.1360 Precautions	1				1			1		1					1		1	
8 25 1362 Electrical	1				1			1		1					1		1	
supplies for emergency																		
conditions.	1				1			1		1					1		1	
§ 25.1363 Electrical																		
system tests.	1				1			1		1					1		1	
§ 25.1365 Electrical																		
appliances, motors, and															_			
transformers.	1		ale.		1			1		1					1		1	
T • 1 /	* *		~ *															
Lights \$ 25,1291 Instrument	*		*															
§ 25.1581 Instrument			1															
§ 25.1383 Landing lights.			1															

	Ic Dula	Applicable to	UAV :	DA Fleet	History	Applicability		Flight Test			Ground Test / Inspection		Anloreio/	Drawings Drawings	NEVIEW	Work Needed	loverage	erage
	Complete	No	Partial	Complete	No	Partial	Complete	No	Partial	Complete	No	Partial	Complete	No	Partial	Additional	Complete (Partial Cov
§ 25.1385 Position light																		
system installation.	1				1			1		1			1				1	
§ 25.1387 Position light system dihedral angles.	1				1			1		1			1				1	
§ 25.1389 Position light distribution and intensities.	1				1			1		1			1				1	
§ 25.1391 Minimum intensities in the horizontal plane of forward and rear position lights.	1				1			1		1			1				1	
§ 25.1393 Minimum intensities in any vertical plane of forward and rear position lights.	1				1			1		1			1				1	
§ 25.1395 Maximum intensities in overlapping beams of forward and rear								_										
position lights.	1				1			1		1			1				1	
§ 25.1397 Colorspecifications.§ 25.1399 Riding light.	1		1		1			1		1			1				1	

	Ic Dulo	Applicable to	UAV :	DA Floot	History	Applicability		Flight Test			Ground Test / Inspection		Anlausi s/	Drawings	Keview	Work Needed	overage	erage
	Complete	No	Partial	Complete	No	Partial	Complete	No	Partial	Complete	No	Partial	Complete	No	Partial	Additional	Complete C	Partial Cov
§ 25.1401 Anticollision light system.	1				1			1		1			1				1	
§ 25.1403 Wing icing																		
detection lights.			1															
	*		*															
Safety Equipment	*		*															
§ 25.1411 General.			1															
§ 25.1415 Ducning			1															
§ 25.1419 Ice protection.			1															
§ 25.1421 Megaphones.			1															
§ 25.1423 Public address																		
system.			1															
	*		*															

L _c Dulo	Applicable to	UAV (History	Applicability		Flight Test			Ground Test / Inspection		Anlaweie/	Drawings	Kevlew	Work Needed	Coverage	erage	
Complete	No	Partial	Complete	No	Partial	Complete	No	Partial	Complete	No	Partial	Complete	No	Partial	Additional	Complete C	Partial Cov	
*		*																
Ŷ		Ť																
1				1				1	1					1		1		
-				-				-	-					-		-		
1				1		1			1					1		1		
1				1		1			1					1		1		
1				I		1			1					1		I		
		1																
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	1 * Complete	1 1 1 1	ICompleteII<	L Complete I I I I I I I I I I I I I	1 Complete 1 No 1 No 1 1	1 1 * Complete 1 1 1 1 1	Londer Laboration	1 Complete Is Rule 1 No Applicable to 1 N No 1 N No 1 N No 1 N No 1 No History 1 No History 1 No History 1 No Flight Test No Flight Test	1 1 * Complete 1 1 * No Applicable to 1 1 1 * No Applicable to 1 1 1 * Partial No Applicable to 1 1 1 * No Applicable to No Applicable to 1 1 1 1 * No Applicable to No Partial No History 1 1 1 1 No No History Applicability 1 1 1 1 No No History Applicability 1 1 1 No No History Applicability 1 1 1 1 No Fisht Test No Fisht Test 1 No Fisht Test No Fisht Test No Fisht Test	1 1 * Complete 1 1 No Applicable to No 1 1 1 No 1 1 1	1 1 * Complete Is Rule 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	1 1	I I I I I I I IS Rule I I I I I No Applicable to I I I I I I IS Rule I I I I I IS Rule I I I I I IS Rule I I I I I IS NO I I I I IS NO ISIN I I I I ISIN ISIN I I I	Image:	1 1 1 1 * Complete Is Rule 1 1 1 1 × Partial No Applicable to 1 1 1 1 1 × Partial No No 1 1 1 1 1 No Partial Partial 1 1 1 1 No Partial Partial Partial 1 1 1 1 No Partial Partial Partial Partial Partial 1 1 1 1 No Partial Partial <td>$\begin{array}{cccccccccccccccccccccccccccccccccccc$</td> <td>$\begin{array}{c ccccccccccccccccccccccccccccccccccc$</td>	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	
	La Dula	Applicable to		DA Fileat	History	Applicability		Flight Test			Ground Test / Inspection		Anlaweie/	Drawings	Kevlew	Work Needed	Coverage	erage
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	Complete	No	Partial	Complete	No	Partial	Complete	No	Partial	Complete	No	Partial	Complete	No	Partial	Additional	Complete (Partial Cov
§ 25.1447 Equipment standards for oxygen dispensing units.			1															
§ 25.1449 Means for determining use of oxygen.§ 25.1450 Chemical			1															
\$ 25.1453 Protection of			1															
oxygen equipment from rupture. § 25.1455 Draining of			1															
fluids subject to freezing. § 25.1457 Cockpit voice			1															
§ 25.1459 Flight datarecorders.			1															
§ 25.1461 Equipment containing high energy rotors.			1															
	*		*															

	Ic Rula	Applicable to		DA Floot	History	Applicability		Flight Test			Ground Test / Inspection		Anloreic/	Drawings	Kevlew	Work Needed	Coverage	erage
	Complete	No	Partial	Complete	No	Partial	Complete	No	Partial	Complete	No	Partial	Complete	No	Partial	Additional	Complete (Partial Cov
Subpart G—																		
Operating																		
Limitations and																		
Information	*		*															
	*		*															
§ 25.1501 General.	1				1			1		1				1			1	
	*		*															
Operating Limitations	*		*															
§ 25.1503 Airspeed	1				1		1			1				1			1	
s 25 1505 Mayimum	1				1		1			1				1			1	
operating limit speed	1				1		1			1				1			1	
§ 25.1507 Maneuvering	-						-			1							1	
speed.	1				1		1			1				1			1	
§ 25.1511 Flap extended																		
speed.			1															
§ 25.1513 Minimum																		
control speed.	1				1		1			1				1			1	
§ 25.1515 Landing gear speeds.	1				1		1			1				1			1	

	Ic Rule	Applicable to		DA Fleet	History	Аррисаниу		Flight Test			Ground Test / Inspection		Anlaweie/	Drawings	Kevlew	Work Needed	Coverage	erage
	Complete	No	Partial	Complete	No	Partial	Complete	No	Partial	Complete	No	Partial	Complete	No	Partial	Additional	Complete (Partial Cov
§ 25.1516 Other speed																		
limitations.	1				1		1			1				1			1	
§ 25.1517 Rough air speed,																		
VRA.	1				1		1			1				1			1	
§ 25.1519 Weight, center																		
distribution	1				1		1			1				1			1	
8 25 1521 Powerplant	1				1		1			1				1			1	
limitations.	1				1		1			1				1			1	
§ 25.1522 Auxiliary power																		
unit limitations.			1															
§ 25.1523 Minimum flight																		
crew.			1															
§ 25.1525 Kinds of	1				1			1		1				1			1	
8 25 1527 Ambient ein	1				1			1		1				1			1	
§ 25.1527 Amolent air temperature and operating																		
altitude.	1				1		1			1				1			1	
§ 25.1529 Instructions for																		
Continued Airworthiness.	1				1		1			1				1			1	
§ 25.1531 Maneuvering																		
flight load factors.	1				1		1			1				1			1	

	Ic Dula	Applicable to		DA Fleet	History	Аррисаонну		Flight Test			Ground Test / Inspection		A sloveic/	Drawings	Kevlew	Work Needed	Coverage	erage
	Complete	No	Partial	Complete	No	Partial	Complete	No	Partial	Complete	No	Partial	Complete	No	Partial	Additional	Complete (Partial Cov
§ 25.1533 Additionaloperating limitations.§ 25.1535 ETOPS	1				1			1		1				1			1	
approval.	*		1 *															
<i>Markings and Placards</i> § 25.1541 General.	* 1		*		1			1		1				1			1	
§ 25.1543 Instrument markings: general.	1				1			1		1				1			1	
§ 25.1545 Airspeed limitation information.	1				1			1		1				1			1	
§ 25.1547 Magnetic direction indicator.			1															
§ 25.1549 Powerplant and auxiliary power unit			1															
<pre>struments. § 25.1551 Oil quantity</pre>			1															
indication. § 25.1553 Fuel quantity	1				1			1		1				1			1	
indicator. § 25.1555 Control markings.	1		1		1			1		1				1			1	

	Ic Rule	Applicable to		DA Floot	History	Applicability		Flight Test			Ground Test / Inspection		A 11 00010 /	Drawings	Kevlew	Work Needed	Coverage	erage
	Complete	No	Partial	Complete	No	Partial	Complete	No	Partial	Complete	No	Partial	Complete	No	Partial	Additional	Complete (Partial Cov
 § 25.1557 Miscellaneous markings and placards. § 25.1561 Safety equipment. § 25.1563 Airspeed 	1		1		1			1		1				1			1	
placard.	1 *		*		1			1		1				1			1	
Airplane Flight Manual	*		*															
§ 25.1581 General.	1				1			1		1				1			1	
§ 25.1583 Operating limitations.	1				1			1		1				1			1	
§ 25.1585 Operating procedures.	1				1			1		1				1			1	
§ 25.1587 Performance information.	1 *		*		1			1		1				1			1	

	Is Rule	Applicable to UAV?		DA Fleet	History	Аррисаниу		Flight Test			Ground Test / Inspection		/oisueln A	Drawings	Keview	Work Needed	Coverage	'erage
	Complete	No	Partial	Complete	No	Partial	Complete	No	Partial	Complete	No	Partial	Complete	No	Partial	Additional	Complete (Partial Cov
Subpart H— Electrical Wiring																		
Systems (EWIS)	*		* *															
§ 25.1701 Definition.	1				1			1			1			1		0	1	
 § 25.1703 Function and installation: EWIS. § 25.1705 Systems and 	1				1			1		1					1		1	
functions: EWIS.	1				1			1		1					1		1	
§ 25.1707 Systemseparation: EWIS.§ 25.1709 System safety:	1				1			1		1					1		1	
EWIS.	1				1			1		1					1		1	
identification: EWIS. § 25.1713 Fire protection:	1				1			1		1					1		1	
EWIS. § 25.1715 Electrical bonding and protection against static electricity: EWIS	1				1			1		1					1		1	

	Ic Rule	Applicable to		DA Floot	History	Аррисаонну		Flight Test			Ground Test / Inspection		\	Drawings	Kevlew	Work Needed	overage	erage
	Complete	No	Partial	Complete	No	Partial	Complete	No	Partial	Complete	No	Partial	Complete	No	Partial	Additional	Complete (Partial Cov
§ 25.1717 Circuit																		
protective devices: EWIS.	1				1			1		1					1		1	
§ 25.1719 Accessibility																		
provisions: EWIS.	1				1			1		1					1		1	
§ 25.1721 Protection of	1				1			1		1					1		1	
EWIS.	1				1			1		1					1		1	
§ 25.1/23 Flammable fluid fire protection: EWIS	1				1			1		1					1		1	
§ 25.1725 Powerplants:	1							1		•					1		1	
EWIS.	1				1			1		1					1		1	
§ 25.1727 Flammable fluid																		
shutoff means: EWIS.	1				1			1		1					1		1	
§ 25.1729 Instructions for Continued Airworthiness: EWIS.	1				1			1		1					1		1	
§ 25.1731 Powerplant and																		
APU fire detector system: EWIS.	1				1			1		1					1		1	
§ 25.1733 Fire detector systems, general: EWIS.	1				1			1		1					1		1	

		Is Rule Applicable to	UAV?		DA Fleet History	Applicability		Flight Test			Ground Test /	Horrordent		Anlaysis/ Drawings	Review	Work Needed	Coverage	erage
	Complete	No	Partial	Complete	No	Partial	Complete	No	Partial	Complete	No	Partial	Complete	No	Partial	Additional	Complete (Partial Cov
TOTAL	282	0	115	1	279	7	151	116	15	172	83	27	19	28	235	13	263	S
	71.0%	0.0%	29.0%	0.4%	98.9%	0.7%	53.5%	41.1%	5.3%	61.0%	29.4%	9.6%	6.7%	9.6%	83.3%	4.6%	93.6%	1.8%

Table A.1 – Assessment of Part 25 Applicability to UAS and Sufficiency of Compliance Means

	LL	RP	HL	RE	===	PWP	AP	EE	HD	STR	ME	PE	ENV
2000	1	3	3	0	0	0	0	0	0	0	0	0	0
2001	0.5	0	4	6.5	1	3	2	1	1	0	0	0	0
2002	1.0	1	2	11	0	6	3	1	1	0	0	0	1
2003	0	1	1	10	3	4	4	0	1	1	0	0	0
2004	0	2	3	8	2	5	3	0	0	0	2	0	0
2005	1	2	4	12	1	7	5	0	0	0	0	0	0
2006	1	4	2	13	2	9	2	2	0	0	0	0	0
2007	2	2	4	13	0	9	1	2	0	1	0	1	1
2008	3	10	11	25	0	18	5	0	0	2	1	1	5
2009	3	10	9	35	0	23	4	6	1	1	2	1	5
SUM	12.5	35	43	133.5	9	84	29	12	4	5	5	3	12
4.9%	13.8%	17.0%	52.8%	3.6%	33.2%	11.5%	4.7%	1.6%	2.0%	2.0%	1.2%	4.7%	4.9%
		Remote	47.2%		Non-Remote	49.4%							

Appendix B: Summary Data – AFSC – All Classes

Table B.1 – Fleet Cause Mishap Frequency – All Classes – AFSC

	LL	RP	HL	RE	===	PWP	AP	EE	HD	STR	ME	PE	ENV
2000	1	3	3	0	0	0	0	0	0	0	0	0	0
2001	1.5	3	7	6.5	1	3	2	1	1	0	0	0	0
2002	2.5	4	9	17.5	1	9	5	2	2	0	0	0	1
2003	2.5	5	10	27.5	4	13	9	2	3	1	0	0	1
2004	2.5	7	13	35.5	6	18	12	2	3	1	2	0	1
2005	3.5	9	17	47.5	7	25	17	2	3	1	2	0	1
2006	4.5	13	19	60.5	9	34	19	4	3	1	2	0	1
2007	6.5	15	23	73.5	9	43	20	6	3	2	2	1	2
2008	9.5	25	34	98.5	9	61	25	6	3	4	3	2	7
2009	12.5	35	43	133.5	9	84	29	12	4	5	5	3	12

Table B.2 – Fleet Cause Accrued Mishaps – All Classes – AFSC

	LL	RP	HL	RE	===	PWP	AP	EE	HD	STR	ME	PE	ENV
2001	1.9E-04	3.7E-04	8.7E-04	8.0E-04	1.2E-04	3.7E-04	2.5E-04	1.2E-04	1.2E-04	0.0E+00	0.0E+00	0.0E+00	0.0E+00
2002	8.6E-05	1.4E-04	3.1E-04	6.0E-04	3.4E-05	3.1E-04	1.7E-04	6.9E-05	6.9E-05	0.0E+00	0.0E+00	0.0E+00	3.4E-05
2003	4.9E-05	9.9E-05	2.0E-04	5.4E-04	7.9E-05	2.6E-04	1.8E-04	4.0E-05	5.9E-05	2.0E-05	0.0E+00	0.0E+00	2.0E-05
2004	3.0E-05	8.3E-05	1.5E-04	4.2E-04	7.1E-05	2.1E-04	1.4E-04	2.4E-05	3.6E-05	1.2E-05	2.4E-05	0.0E+00	1.2E-05
2005	2.7E-05	6.9E-05	1.3E-04	3.6E-04	5.4E-05	1.9E-04	1.3E-04	1.5E-05	2.3E-05	7.7E-06	1.5E-05	0.0E+00	7.7E-06
2006	2.3E-05	6.7E-05	9.8E-05	3.1E-04	4.6E-05	1.7E-04	9.8E-05	2.1E-05	1.5E-05	5.1E-06	1.0E-05	0.0E+00	5.1E-06
2007	2.3E-05	5.2E-05	8.0E-05	2.6E-04	3.1E-05	1.5E-04	7.0E-05	2.1E-05	1.0E-05	7.0E-06	7.0E-06	3.5E-06	7.0E-06
2008	2.1E-05	5.5E-05	7.5E-05	2.2E-04	2.0E-05	1.3E-04	5.5E-05	1.3E-05	6.6E-06	8.8E-06	6.6E-06	4.4E-06	1.5E-05
2009	1.9E-05	5.2E-05	6.4E-05	2.0E-04	1.3E-05	1.2E-04	4.3E-05	1.8E-05	5.9E-06	7.4E-06	7.4E-06	4.4E-06	1.8E-05

Table B.3 – Fleet Cause Accrued Mishap Rate – All Classes – AFSC

	RQ-1 /MQ-1	MQ-9	RQ-4	SUM
2001	7,571	30	486	8,087
2002	19,313	191	1,566	21,070
2003	20,507	100	779	21,386
2004	31,383	767	1,375	33,525
2005	41,024	2,373	2,841	46,238
2006	57,798	3,180	3,214	64,192
2007	79,193	6,872	5,631	91,696
2008	147,980	13,490	7,894	169,364
2009	186,010	26,072	7,810	219,892

Table B.4 - Vehicle Flight Hours - All Classes - AFSC

	RQ-1/ MQ-1	MQ-9	RQ-4	SUM
2001	7,571	30	486	8,087
2002	26,884	221	2,052	29,157
2003	47,391	321	2831	50,543
2004	78,774	1088	4,206	84,068
2005	119,798	3,461	7,047	130,306
2006	177,596	6,641	10,261	194,498
2007	256,789	13,513	15,892	286,194
2008	404,769	27,003	23,786	455,558
2009	590,779	53,075	31,596	675,450

Table B.5 – Vehicle Accrued Flight Hours – All Classes – AFSC

	GCS	MQ-1	MQ-9	RQ-1	RQ-4	SUM
2000	0	0	0	6	1	13
2001	0	1	0	11	0	12
2002	0	2	0	12	2	16
2003	0	1	1	12	1	15
2004	0	12	0	4	1	17
2005	0	15	1	0	4	20
2006	1	16	3	0	2	22
2007	0	18	4	0	1	23
2008	2	42	11	0	1	56
2009	0	47	14	0	4	65
SUM	3	154	34	45	17	253

Table B.6 – Vehicle Mishaps – All Classes – AFSC

	RQ-1/ MQ-1	MQ-9	RQ-4
2001	18	0	1
2002	32	0	3
2003	45	1	4
2004	61	1	5
2005	76	2	9
2006	92	5	11
2007	110	9	12
2008	152	20	13
2009	199	34	17

Table B.7 - Vehicle Accured Mishaps - All Classes - AFSC

	Α	В	С	D	Е
2000	2	1	3	0	1
2001	4	1	4	0	3
2002	9	0	5	0	2
2003	2	0	3	0	10
2004	6	0	4	0	7
2005	10	2	2	0	6
2006	7	0	4	0	11
2007	8	0	3	0	12
2008	13	3	18	0	22
2009	18	4	15	0	28
SUM	79	11	61	0	102

Table B.8 – Class Mishaps – AFSC

	RQ-1 / MQ-1	MQ-9	RQ-4
2000	5	0	0
2001	8	0	0
2002	7	0	0
2003	11	1	1
2004	10	0	1
2005	5	1	4
2006	11	1	2
2007	11	3	1
2008	32	8	1
2009	34	10	3
SUM	134	24	13

Table B.9 – Vehicle Mishaps – Classes B-E – AFSC

	RQ-1 / MQ-1	MQ-9	RQ-4
2000	5	0	0
2001	13	0	0
2002	20	0	0
2003	31	1	1
2004	41	1	2
2005	46	2	6
2006	57	3	8
2007	68	6	9
2008	100	14	10
2009	134	24	13

Table B.10 - Vehicle Accrued Mishaps - Classes B-E - AFSC

	RQ-1 /MQ-1	MQ-9	RQ-4
2001	2.4E-03	0.0E+00	2.1E-03
2002	1.2E-03	0.0E+00	1.5E-03
2003	9.5E-04	3.1E-03	1.4E-03
2004	7.7E-04	9.2E-04	1.2E-03
2005	6.3E-04	5.8E-04	1.3E-03
2006	5.2E-04	7.5E-04	1.1E-03
2007	4.3E-04	6.7E-04	7.6E-04
2008	3.8E-04	7.4E-04	5.5E-04
2009	3.4E-04	6.4E-04	5.4E-04

Table B.11 – Vehicle Accrued Mishap Rate – All Classes – AFSC

	RQ-1 / MQ-1	MQ-9	RQ-4
2001	1.7E-03	0.0E+00	0.0E+00
2002	1.0E-03	0.0E+00	0.0E+00
2003	1.5E-03	1.0E-02	1.3E-03
2004	1.3E-03	1.3E-03	1.5E-03
2005	1.1E-03	8.4E-04	2.1E-03
2006	9.9E-04	9.4E-04	2.5E-03
2007	8.6E-04	8.7E-04	1.6E-03
2008	6.8E-04	1.0E-03	1.3E-03
2009	7.2E-04	9.2E-04	1.7E-03

Table B.12 – Vehicle Accrued Mishaps Rates – Classes B-E – AFSC

	LL	RP	HL	RE	===	PWP	AP	EE	HD	STR	ME	PE	ENV
2000	1	2	3	0	0	0	0	0	0	0	0	0	0
2001	0.5	0	4	6.5	1	3	2	1	1	0	0	0	0
2002	1.0	0	2	10	0	5	3	1	1	0	0	0	1
2003	0	1	0	9	3	3	4	0	1	1	0	0	0
2004	0	2	3	7	2	5	2	0	0	0	2	0	0
2005	1	2	2	9	1	4	5	0	0	0	0	0	0
2006	1	2	1	10	2	8	1	1	0	0	0	0	0
2007	2	0	3	12	0	8	1	2	0	1	0	0	1
2008	2	9	5	22	0	15	5	0	0	2	1	0	3
2009	2	7	7	25	0	19	3	2	0	1	2	1	3
SUM	10.5	25	30	110.5	9	70	26	7	3	5	5	1	8
	5.3%	12.6%	15.1%	55.5%	4.5%	35.2%	13.1%	3.5%	1.5%	2.5%	2.5%	0.5%	4.0%
			Remote	46.0%		Non-Remote	49.7%						

Table B.13 - RQ-1 / MQ-1 Cause Mishap Frequency - All Classes - AFSC

	LL	RP	HL	RE	===	PWP	AP	EE	HD	STR	ME	PE	ENV
2000	1	2	3	0	0	0	0	0	0	0	0	0	0
2001	1.5	2	7	6.5	1	3	2	1	1	0	0	0	0
2002	2.5	2	9	16.5	1	8	5	2	2	0	0	0	1
2003	2.5	3	9	25.5	4	11	9	2	3	1	0	0	1
2004	2.5	5	12	32.5	6	16	11	2	3	1	2	0	1
2005	3.5	7	14	41.5	7	20	16	2	3	1	2	0	1
2006	4.5	9	15	51.5	9	28	17	3	3	1	2	0	1
2007	6.5	9	18	63.5	9	36	18	5	3	2	2	0	2
2008	8.5	18	23	85.5	9	51	23	5	3	4	3	0	5
2009	10.5	25	30	110.5	9	70	26	7	3	5	5	1	8

Table B.14 - RQ-1 / MQ-1 Cause Accrued Mishaps - All Classes - AFSC

	LL	RP	HL	RE	===	PWP	AP	EE	HD	STR	ME	PE	ENV
2001	2.0E-04	2.6E-04	9.2E-04	8.6E-04	1.3E-04	4.0E-04	2.6E-04	1.3E-04	1.3E-04	0.0E+00	0.0E+00	0.0E+00	0.0E+00
2002	9.3E-05	7.4E-05	3.3E-04	6.1E-04	3.7E-05	3.0E-04	1.9E-04	7.4E-05	7.4E-05	0.0E+00	0.0E+00	0.0E+00	3.7E-05
2003	5.3E-05	6.3E-05	1.9E-04	5.4E-04	8.4E-05	2.3E-04	1.9E-04	4.2E-05	6.3E-05	2.1E-05	0.0E+00	0.0E+00	2.1E-05
2004	3.2E-05	6.3E-05	1.5E-04	4.1E-04	7.6E-05	2.0E-04	1.4E-04	2.5E-05	3.8E-05	1.3E-05	2.5E-05	0.0E+00	1.3E-05
2005	2.9E-05	5.8E-05	1.2E-04	3.5E-04	5.8E-05	1.7E-04	1.3E-04	1.7E-05	2.5E-05	8.3E-06	1.7E-05	0.0E+00	8.3E-06
2006	2.5E-05	5.1E-05	8.4E-05	2.9E-04	5.1E-05	1.6E-04	9.6E-05	1.7E-05	1.7E-05	5.6E-06	1.1E-05	0.0E+00	5.6E-06
2007	2.5E-05	3.5E-05	7.0E-05	2.5E-04	3.5E-05	1.4E-04	7.0E-05	1.9E-05	1.2E-05	7.8E-06	7.8E-06	0.0E+00	7.8E-06
2008	2.1E-05	4.4E-05	5.7E-05	2.1E-04	2.2E-05	1.3E-04	5.7E-05	1.2E-05	7.4E-06	9.9E-06	7.4E-06	0.0E+00	1.2E-05
2009	1.8E-05	4.2E-05	5.1E-05	1.9E-04	1.5E-05	1.2E-04	4.4E-05	1.2E-05	5.1E-06	8.5E-06	8.5E-06	1.7E-06	1.4E-05

Table B.15 – RQ-1 / MQ-1 Cause Accrued Mishap Rate – All Classes – AFSC

	LL	RP	HL	RE	=====	PWP	AP	EE	HD	STR	ME	PE	ENV
2000	0	1	0	0	0	0	0	0	0	0	0	0	0
2001	0	0	0	0	0	0	0	0	0	0	0	0	0
2002	0	1	0	1	0	1	0	0	0	0	0	0	0
2003	0	0	0	1	0	1	0	0	0	0	0	0	0
2004	0	0	0	1	0	0	1	0	0	0	0	0	0
2005	0	0	1	3	0	3	0	0	0	0	0	0	0
2006	0	0	0	2	0	1	1	0	0	0	0	0	0
2007	0	0	0	0	0	0	0	0	0	0	0	1	0
2008	1	0	0	0	0	0	0	0	0	0	0	0	0
2009	0	1	0	3	0	0	0	2	1	0	0	0	0
SUM	1	3	1	11	0	6	2	2	1	0	0	1	0
	5.9%	17.6%	5.9%	64.7%	0.0%	35.3%	11.8%	11.8%	5.9%	0.0%	0.0%	5.9%	0.0%
			Remote	41.2%		Non-Remote	8.8%						

Table B.16 – RQ-4 Cause Mishap Frequency – All Classes – AFSC

	LL	RP	HL	RE	===	PWP	AP	EE	HD	STR	ME	PE	ENV
2000	0	1	0	0	0	0	0	0	0	0	0	0	0
2001	0	1	0	0	0	0	0	0	0	0	0	0	0
2002	0	2	0	1	0	1	0	0	0	0	0	0	0
2003	0	2	0	2	0	2	0	0	0	0	0	0	0
2004	0	2	0	3	0	2	1	0	0	0	0	0	0
2005	0	2	1	6	0	5	1	0	0	0	0	0	0
2006	0	2	1	8	0	6	2	0	0	0	0	0	0
2007	0	2	1	8	0	6	2	0	0	0	0	1	0
2008	1	2	1	8	0	6	2	0	0	0	0	1	0
2009	1	3	1	11	0	6	2	2	1	0	0	1	0

Table B.17 – RQ-4 Cause Accrued Mishaps – All Classes – AFSC

	LL	RP	HL	RE	=====	PWP	AP	EE	HD	STR	ME	PE	ENV
2001	0.0E+00	3.3E-02	0.0E+00										
2002	0.0E+00	9.0E-03	0.0E+00	4.5E-03	0.0E+00	4.5E-03	0.0E+00						
2003	0.0E+00	6.2E-03	0.0E+00	6.2E-03	0.0E+00	6.2E-03	0.0E+00						
2004	0.0E+00	1.8E-03	0.0E+00	2.8E-03	0.0E+00	1.8E-03	9.2E-04	0.0E+00	0.0E+00	0.0E+00	0.0E+00	0.0E+00	0.0E+00
2005	0.0E+00	5.8E-04	2.9E-04	1.7E-03	0.0E+00	1.4E-03	2.9E-04	0.0E+00	0.0E+00	0.0E+00	0.0E+00	0.0E+00	0.0E+00
2006	0.0E+00	3.0E-04	1.5E-04	1.2E-03	0.0E+00	9.0E-04	3.0E-04	0.0E+00	0.0E+00	0.0E+00	0.0E+00	0.0E+00	0.0E+00
2007	0.0E+00	1.5E-04	7.4E-05	5.9E-04	0.0E+00	4.4E-04	1.5E-04	0.0E+00	0.0E+00	0.0E+00	0.0E+00	7.4E-05	0.0E+00
2008	3.7E-05	7.4E-05	3.7E-05	3.0E-04	0.0E+00	2.2E-04	7.4E-05	0.0E+00	0.0E+00	0.0E+00	0.0E+00	3.7E-05	0.0E+00
2009	1.9E-05	5.7E-05	1.9E-05	2.1E-04	0.0E+00	1.1E-04	3.8E-05	3.8E-05	1.9E-05	0.0E+00	0.0E+00	1.9E-05	0.0E+00

Table B.18 – RQ-4 Cause Accrued Mishap Rate – All Classes – AFSC

	LL	RP	HL	RE	=====	PWP	AP	EE	HD	STR	ME	PE	ENV
2000	0	0	0	0	0	0	0	0	0	0	0	0	0
2001	0	0	0	0	0	0	0	0	0	0	0	0	0
2002	0	0	0	0	0	0	0	0	0	0	0	0	0
2003	0	0	1	0	0	0	0	0	0	0	0	0	0
2004	0	0	0	0	0	0	0	0	0	0	0	0	0
2005	0	0	1	0	0	0	0	0	0	0	0	0	0
2006	0	2	1	0	0	0	0	0	0	0	0	0	0
2007	0	2	1	1	0	1	0	0	0	0	0	0	0
2008	0	1	6	3	0	3	0	0	0	0	0	0	1
2009	1	2	2	7	0	4	1	2	0	0	0	0	2
SUM	1	7	12	11	0	8	1	2	0	0	0	0	3
	2.9%	20.6%	35.3%	32.4%	0.0%	23.5%	2.9%	5.9%	0.0%	0.0%	0.0%	0.0%	8.8%
			Remote	61.8%		Non-Remote	38.2%						

Table B.19 – MQ-9 Cause Mishap Frequency – All Classes – AFSC

	LL	RP	HL	RE	===	PWP	AP	EE	HD	STR	ME	PE	ENV
2000	0	0	0	0	0	0	0	0	0	0	0	0	0
2001	0	0	0	0	0	0	0	0	0	0	0	0	0
2002	0	0	0	0	0	0	0	0	0	0	0	0	0
2003	0	0	1	0	0	0	0	0	0	0	0	0	0
2004	0	0	1	0	0	0	0	0	0	0	0	0	0
2005	0	0	2	0	0	0	0	0	0	0	0	0	0
2006	0	2	3	0	0	0	0	0	0	0	0	0	0
2007	0	4	4	1	0	1	0	0	0	0	0	0	0
2008	0	5	10	4	0	4	0	0	0	0	0	0	1
2009	1	7	12	11	0	8	1	2	0	0	0	0	3

Table B.20 – MQ-9 Cause Accrued Mishaps – All Classes – AFSC

	LL	RP	HL	RE	=====	PWP	AP	EE	HD	STR	ME	PE	ENV
2001	0.0E+00												
2002	0.0E+00												
2003	0.0E+00	0.0E+00	3.1E-03	0.0E+00									
2004	0.0E+00	0.0E+00	9.2E-04	0.0E+00									
2005	0.0E+00	0.0E+00	5.8E-04	0.0E+00									
2006	0.0E+00	3.0E-04	4.5E-04	0.0E+00									
2007	0.0E+00	3.0E-04	3.0E-04	7.4E-05	0.0E+00	7.4E-05	0.0E+00						
2008	0.0E+00	1.9E-04	3.7E-04	1.5E-04	0.0E+00	1.5E-04	0.0E+00	0.0E+00	0.0E+00	0.0E+00	0.0E+00	0.0E+00	3.7E-05
2009	1.9E-05	1.3E-04	2.3E-04	2.1E-04	0.0E+00	1.5E-04	1.9E-05	3.8E-05	0.0E+00	0.0E+00	0.0E+00	0.0E+00	5.7E-05

Table B.21 – MQ-9 Accrued Cause Mishaps – All Classes – AFSC

LL	RP	HL	RE	=====	PWP	AP	EE	HD	STR	ME	PE	ENV
1	1	0	0	0	0	0	0	0	0	0	0	0
0.0	0	1	3.0	0	1	1	1	0	0	0	0	0
1.0	1	1	5	0	3	1	1	0	0	0	0	1
0	1	0	1	0	1	0	0	0	0	0	0	0
0	2	0	4	0	2	2	0	0	0	0	0	0
1	1	2	6	0	3	3	0	0	0	0	0	0
1	1	2	3	0	2	0	1	0	0	0	0	0
1	0	2	5	0	4	0	1	0	0	0	0	0
1	1	5	6	0	4	2	0	0	0	0	0	0
2	2	3	11	0	7	2	2	0	0	0	0	0
8	10	16	44	0	27	11	6	0	0	0	0	1
0	0	0	0	0	0	0	0	0	0	0	0	0
10.1%	12.7%	20.3%	55.7%	0.0%	34.2%	13.9%	7.6%	0.0%	0.0%	0.0%	0.0%	1.3%
	LL 1 0.0 1.0 0 1 1 1 1 1 2 8 0 10.1%	LL RP 1 1 0.0 0 1.0 1 0 1 0 2 1 1 1 1 1 1 1 1 1 1 1 1 2 2 8 10 0 0 10.1% 12.7%	LL RP HL 1 1 0 0.0 0 1 1.0 1 1 0 1 1 0 1 0 0 2 0 1 1 2 1 1 2 1 1 2 1 0 2 1 1 2 1 1 5 2 2 3 8 10 16 0 0 0 10.1% 12.7% 20.3%	LLRPHLRE11000.0013.01.0115010102041126112310251156223118101644000010.1%12.7%20.3%55.7%	LLRPHLRE=====110000.0013.001.01150010100204011260112301025011560223110810164400000010.1%12.7%20.3%55.7%0.0%	LLRPHLRE=====PWP1100000.001 3.0 011.0115030101010204021126031123021156041156041156042231107810164402700000010.1%12.7%20.3%55.7%0.0%34.2%	LLRPHLRE=====PWPAP110000000.0013.00111.0115031010101000204022112603311250401156042115604211560422311072810164402711000000010.1%12.7%20.3%55.7%0.0%34.2%13.9%	LLRPHLRE=====PWPAPEE110000000.0013.001111.0115031101010100020402201126033011250401115604201156042022311072281016440271160000000010.1%12.7%20.3%55.7%0.0%34.2%13.9%7.6%	LLRPHLRE=====PWPAPEEHD1100000000.0013.0011101.01150311001010100002040220011260330011250401010250401011560420011560420022311072208101644027116000000000010.1%12.7%20.3%55.7%0.0%34.2%13.9%7.6%0.0%	LLRPHLRE=====PWPAPEEHDSTR1100000000000.0013.001110001.011503110001010100000101010000020402200011260330001125040100115604200011560420002231107220081016440271160000000000000	LLRPHLRE=====PWPAPEEHDSTRME1100000000000.0013.0011100001.01150311000001010100000001010100000020402200001126033000001125040100001156042000011560420000223110722000810164402711600000000000000000	LLRPHLRE=====PWPAPEEHDSTRMEPE11000000000000.0013.00111000001.0115031100000010101000000001010100000000204022000000112603300000011230201000001125040100000115604200000022311072200000022311027116000000000000000000011644027 </td

Appendix C: Summary Data – AFSC – Class A

Table C.1 – Fleet Cause Mishap Frequency – Class A – AFSC

	LL	RP	HL	RE	===	PWP	AP	EE	HD	STR	ME	PE	ENV
2000	1	1	0	0	0	0	0	0	0	0	0	0	0
2001	1	1	1	3	0	1	1	1	0	0	0	0	0
2002	2	2	2	8	0	4	2	2	0	0	0	0	1
2003	2	3	2	9	0	5	2	2	0	0	0	0	1
2004	2	5	2	13	0	7	4	2	0	0	0	0	1
2005	3	6	4	19	0	10	7	2	0	0	0	0	1
2006	4	7	6	22	0	12	7	3	0	0	0	0	1
2007	5	7	8	27	0	16	7	4	0	0	0	0	1
2008	6	8	13	33	0	20	9	4	0	0	0	0	1
2009	8	10	16	44	0	27	11	6	0	0	0	0	1

Table C.2 – Fleet Cause Accrued Mishaps – Class A – AFSC

	LL	RP	HL	RE	=====	PWP	AP	EE	HD	STR	ME	PE	ENV
2001	1.2E-04	1.2E-04	1.2E-04	3.7E-04	0.0E+00	1.2E-04	1.2E-04	1.2E-04	0.0E+00	0.0E+00	0.0E+00	0.0E+00	0.0E+00
2002	6.9E-05	6.9E-05	6.9E-05	2.7E-04	0.0E+00	1.4E-04	6.9E-05	6.9E-05	0.0E+00	0.0E+00	0.0E+00	0.0E+00	3.4E-05
2003	4.0E-05	5.9E-05	4.0E-05	1.8E-04	0.0E+00	9.9E-05	4.0E-05	4.0E-05	0.0E+00	0.0E+00	0.0E+00	0.0E+00	2.0E-05
2004	2.4E-05	5.9E-05	2.4E-05	1.5E-04	0.0E+00	8.3E-05	4.8E-05	2.4E-05	0.0E+00	0.0E+00	0.0E+00	0.0E+00	1.2E-05
2005	2.3E-05	4.6E-05	3.1E-05	1.5E-04	0.0E+00	7.7E-05	5.4E-05	1.5E-05	0.0E+00	0.0E+00	0.0E+00	0.0E+00	7.7E-06
2006	2.1E-05	3.6E-05	3.1E-05	1.1E-04	0.0E+00	6.2E-05	3.6E-05	1.5E-05	0.0E+00	0.0E+00	0.0E+00	0.0E+00	5.1E-06
2007	1.7E-05	2.4E-05	2.8E-05	9.4E-05	0.0E+00	5.6E-05	2.4E-05	1.4E-05	0.0E+00	0.0E+00	0.0E+00	0.0E+00	3.5E-06
2008	1.3E-05	1.8E-05	2.9E-05	7.2E-05	0.0E+00	4.4E-05	2.0E-05	8.8E-06	0.0E+00	0.0E+00	0.0E+00	0.0E+00	2.2E-06
2009	1.2E-05	1.5E-05	2.4E-05	6.5E-05	0.0E+00	4.0E-05	1.6E-05	8.9E-06	0.0E+00	0.0E+00	0.0E+00	0.0E+00	1.5E-06

Table C.3 – Fleet Cause Accrued Mishap Rate – Class A – AFSC

	GCS	MQ-1	MQ-9	RQ-1	RQ-4	MQ-1/ RQ-1
2000	0	0	0	1	1	1
2001	0	1	0	3	0	4
2002	0	2	0	5	2	7
2003	0	0	0	2	0	2
2004	0	5	0	1	0	6
2005	0	10	0	0	0	10
2006	0	5	2	0	0	5
2007	0	7	1	0	0	7
2008	0	10	3	0	0	10
2009	0	13	4	0	1	13
SUM	0	53	10	12	4	65

Table C.4 – Vehicle Mishap Frequency – Class A – AFSC

	RQ-1/ MQ-1	MQ-9	RQ-4
2000	1	0	1
2001	5	0	1
2002	12	0	3
2003	14	0	3
2004	20	0	3
2005	30	0	3
2006	35	2	3
2007	42	3	3
2008	52	6	3
2009	65	10	4

Table C.5 – Vehicle Accrude Mishaps – Class A – AFSC

	RQ-1/ MQ-1	MQ-9	RQ-4
2001	6.6E-04	0.0E+00	2.1E-03
2002	4.5E-04	0.0E+00	1.5E-03
2003	3.0E-04	0.0E+00	1.1E-03
2004	2.5E-04	0.0E+00	7.1E-04
2005	2.5E-04	0.0E+00	4.3E-04
2006	2.0E-04	3.0E-04	2.9E-04
2007	1.6E-04	2.2E-04	1.9E-04
2008	1.3E-04	2.2E-04	1.3E-04
2009	1.1E-04	1.9E-04	1.3E-04

Table C.6 – Vehicle Mishap Rate – Class A – AFSC

	LL	RP	HL	RE	=====	PWP	AP	EE	HD	STR	ME	PE	ENV
2000	1	0	0	0	0	0	0	0	0	0	0	0	0
2001	0	0	1	3	0	1	1	1	0	0	0	0	0
2002	1	0	1	4	0	2	1	1	0	0	0	0	1
2003	0	1	0	1	0	1	0	0	0	0	0	0	0
2004	0	2	0	4	0	2	2	0	0	0	0	0	0
2005	1	1	2	6	0	3	3	0	0	0	0	0	0
2006	1	0	1	3	0	2	0	1	0	0	0	0	0
2007	1	0	1	5	0	4	0	1	0	0	0	0	0
2008	1	1	2	6	0	4	2	0	0	0	0	0	0
2009	1	1	2	9	0	5	2	2	0	0	0	0	0
SUM	7	6	10	41	0	24	11	6	0	0	0	0	1
	10.8%	9.2%	15.4% Remote	63.1% 52.3%	0.0%	36.9% Non-Remote	16.9% 47.7%	9.2%	0.0%	0.0%	0.0%	0.0%	1.5%

Table C.7 – RQ-1 / MQ-1 Cause Mishap Frequency – Class A – AFSC

	LL	RP	HL	RE	===	PWP	AP	EE	HD	STR	ME	PE	ENV
2000	1	0	0	0	0	0	0	0	0	0	0	0	0
2001	1	0	1	3	0	1	1	1	0	0	0	0	0
2002	2	0	2	7	0	3	2	2	0	0	0	0	1
2003	2	1	2	8	0	4	2	2	0	0	0	0	1
2004	2	3	2	12	0	6	4	2	0	0	0	0	1
2005	3	4	4	18	0	9	7	2	0	0	0	0	1
2006	4	4	5	21	0	11	7	3	0	0	0	0	1
2007	5	4	6	26	0	15	7	4	0	0	0	0	1
2008	6	5	8	32	0	19	9	4	0	0	0	0	1
2009	7	6	10	41	0	24	11	6	0	0	0	0	1

Table C.8 – RQ-1 / MQ-1 Cause Accrued Mishaps – Class A – AFSC

	LL	RP	HL	RE	=====	PWP	AP	EE	HD	STR	ME	PE	ENV
2001	1.3E-04	0.0E+00	1.3E-04	4.0E-04	0.0E+00	1.3E-04	1.3E-04	1.3E-04	0.0E+00	0.0E+00	0.0E+00	0.0E+00	0.0E+00
2002	7.4E-05	0.0E+00	7.4E-05	2.6E-04	0.0E+00	1.1E-04	7.4E-05	7.4E-05	0.0E+00	0.0E+00	0.0E+00	0.0E+00	3.7E-05
2003	4.2E-05	2.1E-05	4.2E-05	1.7E-04	0.0E+00	8.4E-05	4.2E-05	4.2E-05	0.0E+00	0.0E+00	0.0E+00	0.0E+00	2.1E-05
2004	2.5E-05	3.8E-05	2.5E-05	1.5E-04	0.0E+00	7.6E-05	5.1E-05	2.5E-05	0.0E+00	0.0E+00	0.0E+00	0.0E+00	1.3E-05
2005	2.5E-05	3.3E-05	3.3E-05	1.5E-04	0.0E+00	7.5E-05	5.8E-05	1.7E-05	0.0E+00	0.0E+00	0.0E+00	0.0E+00	8.3E-06
2006	2.3E-05	2.3E-05	2.8E-05	1.2E-04	0.0E+00	6.2E-05	3.9E-05	1.7E-05	0.0E+00	0.0E+00	0.0E+00	0.0E+00	5.6E-06
2007	1.9E-05	1.6E-05	2.3E-05	1.0E-04	0.0E+00	5.8E-05	2.7E-05	1.6E-05	0.0E+00	0.0E+00	0.0E+00	0.0E+00	3.9E-06
2008	1.5E-05	1.2E-05	2.0E-05	7.9E-05	0.0E+00	4.7E-05	2.2E-05	9.9E-06	0.0E+00	0.0E+00	0.0E+00	0.0E+00	2.5E-06
2009	1.2E-05	1.0E-05	1.7E-05	6.9E-05	0.0E+00	4.1E-05	1.9E-05	1.0E-05	0.0E+00	0.0E+00	0.0E+00	0.0E+00	1.7E-06

Table C.9 – RQ-1 / MQ-1 Cause Accrued Mishap Rate – Class A – AFSC

	LL	RP	HL	RE - PWP	=====	PWP	AP	EE	HD	STR	ME	PE	ENV
2000	0	1	0	0	0	0	0	0	0	0	0	0	0
2001	0	0	0	0	0	0	0	0	0	0	0	0	0
2002	0	1	0	1	0	1	0	0	0	0	0	0	0
2003	0	0	0	0	0	0	0	0	0	0	0	0	0
2004	0	0	0	0	0	0	0	0	0	0	0	0	0
2005	0	0	0	0	0	0	0	0	0	0	0	0	0
2006	0	0	0	0	0	0	0	0	0	0	0	0	0
2007	0	0	0	0	0	0	0	0	0	0	0	0	0
2008	0	0	0	0	0	0	0	0	0	0	0	0	0
2009	0	1	0	0	0	0	0	0	0	0	0	0	0
SUM	0	3	0	1	0	1	0	0	0	0	0	0	0
	0.0%	75.0%	0.0% Remote	25.0% 75.0%	0.0%	25.0% Non-Remote	0.0% 25.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%

Table C.10 – RQ-4 Cause Mishap Frequency – Class A – AFSC

	LL	RP	HL	RE	===	PWP	AP	EE	HD	STR	ME	PE	ENV
2000	0	1	0	0	0	0	0	0	0	0	0	0	0
2001	0	1	0	0	0	0	0	0	0	0	0	0	0
2002	0	2	0	1	0	1	0	0	0	0	0	0	0
2003	0	2	0	1	0	1	0	0	0	0	0	0	0
2004	0	2	0	1	0	1	0	0	0	0	0	0	0
2005	0	2	0	1	0	1	0	0	0	0	0	0	0
2006	0	2	0	1	0	1	0	0	0	0	0	0	0
2007	0	2	0	1	0	1	0	0	0	0	0	0	0
2008	0	2	0	1	0	1	0	0	0	0	0	0	0
2009	0	3	0	1	0	1	0	0	0	0	0	0	0

Table C.11 – RQ-4 Cause Accrued Mishaps – Class A - AFSC

	LL	RP	HL	RE	=====	PWP	AP	EE	HD	STR	ME	PE	ENV
2001	0.0E+00	2.1E-03	0.0E+00										
2002	0.0E+00	9.7E-04	0.0E+00	4.9E-04	0.0E+00	4.9E-04	0.0E+00						
2003	0.0E+00	7.1E-04	0.0E+00	3.5E-04	0.0E+00	3.5E-04	0.0E+00						
2004	0.0E+00	4.8E-04	0.0E+00	2.4E-04	0.0E+00	2.4E-04	0.0E+00						
2005	0.0E+00	2.8E-04	0.0E+00	1.4E-04	0.0E+00	1.4E-04	0.0E+00						
2006	0.0E+00	1.9E-04	0.0E+00	9.7E-05	0.0E+00	9.7E-05	0.0E+00						
2007	0.0E+00	1.3E-04	0.0E+00	6.3E-05	0.0E+00	6.3E-05	0.0E+00						
2008	0.0E+00	8.4E-05	0.0E+00	4.2E-05	0.0E+00	4.2E-05	0.0E+00						
2009	0.0E+00	9.5E-05	0.0E+00	3.2E-05	0.0E+00	3.2E-05	0.0E+00						

Table C.12 – RQ-4 Cause Accrued Mishap Rate – Class A - AFSC

	LL	RP	HL	RE - PWP	=====	PWP	AP	EE	HD	STR	ME	PE	ENV
2000	0	0	0	0	0	0	0	0	0	0	0	0	0
2001	0	0	0	0	0	0	0	0	0	0	0	0	0
2002	0	0	0	0	0	0	0	0	0	0	0	0	0
2003	0	0	0	0	0	0	0	0	0	0	0	0	0
2004	0	0	0	0	0	0	0	0	0	0	0	0	0
2005	0	0	0	0	0	0	0	0	0	0	0	0	0
2006	0	1	1	0	0	0	0	0	0	0	0	0	0
2007	0	0	1	0	0	0	0	0	0	0	0	0	0
2008	0	0	3	0	0	0	0	0	0	0	0	0	0
2009	1	0	1	2	0	2	0	0	0	0	0	0	0
SUM	1	1	6	2	0	2	0	0	0	0	0	0	0
	10%	10%	60%	20%	0%	20%	0%	0%	0%	0%	0%	0%	0%
			Remote	80.0%		Non-Remote	20.0%						

Table C.13 – MQ-9 Cause Mishap Frequency – Class A - AFSC

	LL	RP	HL	RE	===	PWP	AP	EE	HD	STR	ME	PE	ENV
2000	0	0	0	0	0	0	0	0	0	0	0	0	0
2001	0	0	0	0	0	0	0	0	0	0	0	0	0
2002	0	0	0	0	0	0	0	0	0	0	0	0	0
2003	0	0	0	0	0	0	0	0	0	0	0	0	0
2004	0	0	0	0	0	0	0	0	0	0	0	0	0
2005	0	0	0	0	0	0	0	0	0	0	0	0	0
2006	0	1	1	0	0	0	0	0	0	0	0	0	0
2007	0	1	2	0	0	0	0	0	0	0	0	0	0
2008	0	1	5	0	0	0	0	0	0	0	0	0	0
2009	1	1	6	2	0	2	0	0	0	0	0	0	0

Table C.14 – MQ-9 Cause Accrued Mishaps – Class A – AFSC

	LL	RP	HL	RE	===	PWP	AP	EE	HD	STR	ME	PE	ENV
2001	0.0E+00												
2002	0.0E+00												
2003	0.0E+00												
2004	0.0E+00												
2005	0.0E+00												
2006	0.0E+00	1.5E-04	1.5E-04	0.0E+00									
2007	0.0E+00	7.4E-05	1.5E-04	0.0E+00									
2008	0.0E+00	3.7E-05	1.9E-04	0.0E+00									
2009	1.9E-05	1.9E-05	1.1E-04	3.8E-05	0.0E+00	3.8E-05	0.0E+00						

Table C.15 – MQ-9 Cause Accrued Mishap Rate – Class A – AFSC

	LL	RP	HL	RE	PWP	AP	EE	HD	STR	ME	PE	ENV
2000	0	0	0	3	0	3	0	0	0	0	0	0
2001	0	0	0	2	1	1	0	0	0	0	0	0
2002	1	0	1	4	2	0	1	0	1	0	1	0
2003	1	0	0	1	1	0	0	0	0	0	0	0
2004	0	0	2	1	0	1	0	0	0	0	1	0
2005	0	0	1	3	2	1	0	0	0	1	0	0
2006	1	0	1	1	0	1	0	0	0	0	1	0
2007	0	0	1	4	3	0	1	0	0	0	0	0
2008	0	0	0	8	2	0	6	0	0	0	0	0
2009	1	0	0	7	4	0	3	0	0	0	2	1
SUM	4	0	6	34	15	7	11	0	1	1	5	1
	8%	0%	12%	67%	29%	14%	22%	0%	2%	2%	10%	2%

Appendix D: Summary Data – AIB – Class A

Remote 33% Non-Remote 67%

Table D.1 – Fleet Cause Mishap Frequency – Class A - AIB

	LL	RP	HL	RE	PWP	AP	EE	HD	STR	ME	PE	ENV
2000	0	0	0	2	0	2	0	0	0	0	0	0
2001	0	0	0	2	1	1	0	0	0	0	0	0
2002	1	0	1	2	1	0	1	0	0	0	1	0
2003	1	0	0	1	1	0	0	0	0	0	0	0
2004	0	0	2	1	0	1	0	0	0	0	1	0
2005	0	0	1	3	2	1	0	0	0	1	0	0
2006	1	0	0	1	0	1	0	0	0	0	1	0
2007	0	0	1	4	3	0	1	0	0	0	0	0
2008	1	0	0	8	2	0	6	0	0	0	0	0
2009	3	0	0	7	4	0	3	0	0	0	1	1
SUM	7	0	5	31	14	6	11	0	0	1	4	1
	15%	0%	11%	67%	30%	13%	24%	0%	0%	2%	9%	2%
			Remote	39%	Non-Remote	67%	_					

Table D.2 – MQ-1/ RQ-1 – Cause Mishap Frequency – Class A – AIB

	LL	RP	HL	RE	PWP	AP	EE	HD	STR	ME	PE	ENV
2000	0	0	0	1	0	1	0	0	0	0	0	0
2001	0	0	0	0	0	0	0	0	0	0	0	0
2002	0	0	0	2	1	0	0	0	1	0	0	0
2003	0	0	0	0	0	0	0	0	0	0	0	0
2004	0	0	0	0	0	0	0	0	0	0	0	0
2005	0	0	0	0	0	0	0	0	0	0	0	0
2006	0	0	0	0	0	0	0	0	0	0	0	0
2007	0	0	0	0	0	0	0	0	0	0	0	0
2008	0	0	0	0	0	0	0	0	0	0	0	0
2009	0	0	0	0	0	0	0	0	0	0	0	0
SUM	0	0	0	3	1	1	0	0	1	0	0	0
	0%	0%	0%	100%	33%	33%	0%	0%	33%	0%	0%	0%
			Remote	33%	Non-Remote	67%						

Table D.3 – RQ-4 – Cause Mishap Frequency – Class A – AIB

	LL	RP	HL	RE	PWP	AP	EE	HD	STR	ME	PE	ENV
2000	0	0	0	0	0	0	0	0	0	0	0	0
2001	0	0	0	0	0	0	0	0	0	0	0	0
2002	0	0	0	0	0	0	0	0	0	0	0	0
2003	0	0	0	0	0	0	0	0	0	0	0	0
2004	0	0	0	0	0	0	0	0	0	0	0	0
2005	0	0	0	0	0	0	0	0	0	0	0	0
2006	0	0	1	0	0	0	0	0	0	0	0	0
2007	0	0	0	0	0	0	0	0	0	0	0	0
2008	0	0	0	0	0	0	0	0	0	0	0	0
2009	0	0	0	0	0	0	0	0	0	0	1	0
SUM	0	0	1	0	0	0	0	0	0	0	1	0
	0%	0%	50%	0%	0%	0%	0%	0%	0%	0%	50%	0%
			Remote	50%	Non-Remote	50%						

Table D.4 – MQ-9 – Cause Mishap Frequency – Class A – AIB